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Influence of mixed feeding rate in a conventional SBR on biological P-removal and granule stability while treating different industrial effluents

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1 **Influence of mixed feeding rate in a conventional SBR on biological P-**  
2 **removal and granule stability while treating different industrial effluents.**

3 Influence of the feeding rate and COD/P ratio on bio-P activity and granule  
4 stability.

5 Hannah Stes<sup>1,2</sup>, Sven Aerts<sup>2</sup>, Michel Caluwe<sup>1</sup>, Jolien D'aes<sup>1</sup>, Flinn De Vleeschauwer<sup>1</sup>,  
6 Thomas Dobbeleers<sup>1</sup>, Piet De Langhe<sup>2</sup>, Filip Kiekens<sup>3</sup>, Jan Dries<sup>1</sup>

7

8 <sup>1</sup> *Research group BioGEM, Bio-Chemical Green Engineering & Materials, Faculty of Applied*  
9 *Engineering, University of Antwerp, Salesianenlaan 90, 2660 Antwerp, Belgium*

10 <sup>2</sup> *Pantarein Water BVBA, Egide Walschaertstraat 22L, 2800 Mechelen, Belgium*

11 <sup>3</sup> *Laboratory of Pharmaceutical Technology and Biopharmacy, Department of*  
12 *Pharmaceutical Science, University of Antwerp, Universiteitsplein 1, 2610 Wilrijk, Belgium.*

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14 Full postal address: University of Antwerp, Salesianenlaan 90, 2660 Antwerp, Belgium.

15 e-mail: [jan.dries2@uantwerpen.be](mailto:jan.dries2@uantwerpen.be); phone number: +32(0)32658872; fax-number: not  
16 available.

17 **Abstract**

18 In this study the influence of the anaerobic mixed feeding rate on granule stability and reactor  
19 performance in a conventional SBR (C-SBR) was investigated while treating various

20 industrial wastewaters. A lab-scale SBR fed with malting wastewater rich in phosphorus, was

21 operated for approx. 250 days which was divided into two periods: (I) mixed pulse feed and

22 (II) prolonged mixed feed. Initially, no bio-P activity was observed. However, by lowering

23 the feeding rate biological P-removal was rapidly established and no effect on the AGS

24 characteristics were observed. Additionally, to investigate the effect of the mixed feeding rate

25 when treating an industrial effluent poor in phosphorus, i.e. brewery wastewater, a lab-scale

26 reactor was operated for approx. 400 days applying different mixed feeding rates.

27 Morphological and molecular analysis indicated that a low substrate concentration promoted

28 the enrichment of anaerobic carbon storing filaments when fed with brewery wastewater.

29 Findings suggest that a prolonged mixed feeding regime can be used as a tool to easily

30 establish bio-P removal in a C-SBR system for the treatment of phosphorus rich wastewaters.

31 It should however be considered that under P-limiting conditions, enrichment of poly-P  
32 storing filaments may occur possibly due to their higher substrate affinity under anaerobic  
33 conditions.

34 Keywords: Biological phosphorus removal; Conventional SBR; Industrial wastewaters;  
35 Mixed feeding rate; Phosphate accumulating organisms (PAO)

## 36 **Introduction**

37 The European brewing sector is a major contributor to the European economy providing up to  
38 2.3 million direct and indirect jobs. The agriculture malting industry provides products and  
39 serves the beer sector. Europe is responsible for one third of the worldwide malt production  
40 resulting in an increased employment within the overall beer sector (Europe Economics &  
41 The brewers of Europe 2016). Globally, efforts are made towards reducing water usage and  
42 carbon footprint. Brewery wastewater typically contains high amounts of easily biodegradable  
43 compounds (Driessen & Vereijken 2003) while wastewater produced by malting activities  
44 typically contains high amounts of particulate matter (Schwarzenbeck et al. 2004).  
45 Successful full-scale applications of the aerobic granular sludge (AGS) technology have been  
46 reported for the treatment of municipal wastewater resulting in a reduction of energy  
47 consumption between 20-40% and a footprint reduction up to 33% (Pronk et al. 2015). Due to  
48 biomass with excellent settling characteristics, sludge separation is improved drastically  
49 resulting in systems with higher biomass concentrations. In addition, simultaneous  
50 nitrification/denitrification (SND) and biological phosphorus removal contribute to the design  
51 of compact AGS bioreactors (STOWA 2013). It is generally considered as an attractive  
52 technology for the treatment of various industrial wastewaters. However, research using  
53 complex and/or particulate wastewaters such as real municipal wastewater (STOWA 2013)  
54 and industrial effluents (Schwarzenbeck et al. 2004; Caluwé et al. 2017; Stes al. 2018) show  
55 that more complex substrates may lead to filamentous outgrowth on the granule surface and  
56 the co-existence of flocculent and granular sludge. Stable aerobic granule formation when  
57 treating industrial wastewaters with a particulate content still remains challenging. The  
58 enrichment of slow growing organisms such as glycogen accumulating organisms (GAO) and  
59 phosphate accumulating organisms (PAO) appears to be critical to obtain stable aerobic  
60 granulation (STOWA 2013). PAOs and GAOs have the ability to anaerobically convert  
61 volatile fatty acids (VFA) into intracellular storage polymers which are used for microbial  
62 growth during aeration. The energy source for anaerobic VFA uptake is different for both  
63 groups of organisms; for PAOs this energy originates primarily from the hydrolysis of the  
64 intracellularly stored poly-P. For GAOs the main energy source results from the degradation  
65 of intracellular glycogen (Oehmen et al. 2007). Tu & Schuller (2013) found that the in-reactor  
66 substrate concentration influenced the PAO-GAO competition, favouring PAO over GAO  
67 when the mixed feeding rate was decreased (synthetic wastewater). It is suggested that PAOs  
68 are able to apply active transport for anaerobic carbon uptake, giving PAOs a competitive

69 advantage when in-reactor substrate concentrations are low (Tu & Schuler 2013).  
70 Accordingly, growth of GAOs is negatively influenced by lowering the feeding rate pointing  
71 out the importance of excess P to allow PAOs to proliferate under these operational  
72 conditions. Based on these findings, it should be considered that a high COD/P ratio of the  
73 brewery wastewater will prevent proliferation of granule forming PAOs due to limited P  
74 availability. At the same time a lower feeding rate will prevent GAO growth due to an  
75 increased energy demand for anaerobic carbon uptake possibly hampering enrichment of  
76 granule forming organisms. The COD/P ratio may therefore have a substantial impact on the  
77 overall granule characteristics when the feeding rate is lowered. Short anaerobic pulse feeding  
78 strategies (several minutes) are mainly tested in lab-scale experiments to promote granulation  
79 (Val del Río et al. 2012, Caluwé et al. 2017; Stes et al. 2018). Applying this pulse feeding  
80 strategy is technically unfeasible in industrial SBR systems due to the enormous required  
81 feeding flows. Inevitably, existing or newly build WWTP will maintain longer mixed feeding  
82 times. This should be considered as an important operational parameter because of the direct  
83 impact on the in-reactor substrate concentration during the anaerobic feeding phase. It is of  
84 high relevance to investigate the influence of a prolonged anaerobic mixed feeding rate on the  
85 overall aerobic granule stability, reactor performance and the bio-P removal activity in an  
86 AGS system. It is assumed that three operational factors will be influencing the GAO/PAO  
87 competition, i.e. (1) the COD/P ratio (Oehmen et al. 2007), (2) the pH (Filipe et al. 2001b)  
88 and (3) the anaerobic mixed feeding rate (Tu & Schuler 2013). As described by Oehmen et al.  
89 (2007) it is generally assumed that a high influent COD/P ratio favours growth of GAO over  
90 PAO due to the limited availability of phosphate. This study focusses on two main objectives.  
91 The influence of the anaerobic mixed feeding rate on the AGS stability, reactor performance  
92 and bio-P activity was investigated while treating (1) an industrial wastewater with a high  
93 phosphorus content, i.e. malting wastewater and (2) and low phosphorus content, i.e. brewery  
94 wastewater. It is hypothesised that when lowering the feeding rate, the bio-P removal activity  
95 will increase when COD/P ratios are low and PAOs are able to proliferate. However,  
96 deterioration of the granular sludge characteristics may occur when the feeding rate is lowered  
97 while treating a wastewater characterised by a high COD/P ratio.

## Material and Methods

### 98 Reactor set-up

99 Two fully automated lab-scale SBRs were used during this study. The SBR fed with malting  
100 wastewater, SBR<sub>M</sub>, had a working volume of 15L (H/D=3.5) and was operated at room  
101 temperature (18-22°C) for approximately 200 days. The SBR<sub>B</sub>, fed with brewery wastewater  
102 had a working volume of 13L (H/D=1.1) and was operated at room temperature (18-22°C) for  
103 400 days. Each reactor was provided with a mechanical stirrer (IKA RW20 digital), a DO  
104 (Endress+Hauser, Oxymax W COS51D) and pH (Endress+Hauser, Orbisint CPS11-7AA21)  
105 sensor and an aeration system consisting of an aeration pump (Ubbink Air 1000) and an air  
106 diffuser at the bottom of the reactor (AngelAqua DY 104-A). A Siemens PLC (LOGO! Logic  
107 Module) was used for process control. Sensor data was recorded and visualized by an  
108 Ecograph T RSG35 graphic display recorder (Endress+Hauser). Monitoring of the DO set-

109 points was done by the same recorder. A schematic overview of the experimental set-up can  
 110 be found in supplementary data I.

### 111 **Industrial wastewaters and seed sludge**

112 The SBR<sub>M</sub> was fed with wastewater from a local malting company. The wastewater used for  
 113 SBR<sub>B</sub> originated from a local brewery/bottling plant. Sufficient nutrient availability in the  
 114 brewery wastewater was ensured by manual dosage of nitrogen (urea, 30%) and phosphorus  
 115 (phosphoric acid, 75%) resulting in a final COD:N:P ratio of approximately 100:2:0.5. To  
 116 avoid clogging of the feeding tubes, all wastewater was sieved (pore size: 1mm) to remove  
 117 grains and large particulate matter. Minimum, maximum and average influent concentrations  
 118 are summarised in **Table 1**.

119 **Table 1** Malting and brewery (incl. N and P dosage) wastewater composition

	COD <sub>t</sub> (mgO <sub>2</sub> .L <sup>-1</sup> )	COD <sub>s</sub> (mgO <sub>2</sub> .L <sup>-1</sup> )	TN (mgN.L <sup>-1</sup> )	TP (mgP.L <sup>-1</sup> )	COD/P	pH	EC (µS/cm)
<b>Malting</b>							
Min	1256	1079	59.6	19.8	36	5.50	1668
Max	3661	3350	118	47.2	165	7.07	3140
Av	2403	1964	85.4	33.7	76	6.38	2289
Stdev	491	443	12.6	7.54	30	0.44	357
<b>Brewery</b>							
Min	1768	1046	23	12.7	90	4.9	802
Max	7934	6430	166	43.7	433	7.2	3280
Av.	4473	3663	77	24.6	200	5.9	1949
Stdev	1212	1160	24	7.7	82	0.6	452

120  
 121 All influent and effluent concentrations were measured using Hach test kits (Mechelen,  
 122 Belgium); total COD (COD<sub>t</sub>) and soluble COD (COD<sub>s</sub>): LCK014, LCK514; TN-N: LCK  
 123 338, LCK138; NH<sub>4</sub><sup>+</sup>-N: LCK305, NO<sub>2</sub><sup>-</sup>-N: LCK342, NO<sub>3</sub><sup>-</sup>-N: LCK339, TP-P: LCK350 and  
 124 LCK348, respectively. All samples were filtered using glass microfibre filters (particle  
 125 retention: 0.6µm, Macherey-Nagel MN GF-3) before measuring the CODs and PO<sub>4</sub><sup>3-</sup>-P  
 126 concentrations. Seed sludge for SBR<sub>M</sub> originated from a parent lab-scale SBR which was  
 127 operated to promote aerobic granulation while treating malting wastewater. An overview of  
 128 the operational parameters of the parent lab-scale SBR can be found in supplementary data II.  
 129 SBR<sub>B</sub> was seeded with flocculent sludge from the existing local WWTP treating the brewery  
 130 wastewater.

### 131 **Reactor operation**

132 In this study, aerobic granulation was promoted by applying a metabolic selection pressure to  
 133 enhance growth of specific groups of slow growing micro-organisms associated with  
 134 successful AGS formation, i.e. PAOs and GAOs. Therefore, an anaerobic feast/aerobic  
 135 famine regime was applied for both SBR systems which is known to favour growth of  
 136 granule forming organisms over floc forming and/or filamentous organisms. The SBR<sub>M</sub> was  
 137 operated for approx. 200 days, divided into two periods based on changes in anaerobic mixed  
 138 feeding rate. The SBR<sub>B</sub> was operated for approx. 400 days during which the feeding rate was  
 139 lowered on day 182. To quantify the difference in feeding rate from a substrate loading point  
 140 of view, the ratio of the organic loading rate (OLR) to the feeding time per cycle, i.e.

141 OLR<sub>feeding</sub>, was calculated using subsequent formula:

$$142 \quad OLR_{feeding} [kg \text{ COD} \cdot m^{-3} \cdot h^{-1}] = \frac{C_{COD,influent} \cdot V_{influent}}{V_{SBR} \cdot t_{feeding}}$$

143 This parameter is introduced to compare different anaerobic mixed feeding rates since it will  
 144 result in different in-reactor substrate concentrations. An overview of the adjustments in SBR  
 145 operation during the experiment are shown in **Table 2**.

146 **Table 2** Different operational conditions considering the SBR cycle

SBR cycle phase	SBR <sub>M</sub>		SBR <sub>B</sub>	
	Period I	Period II	Period I	Period II
	Day 1-85	Day 86-200	Day 1-181	Day 182-400
Mixed idle phase (min)	10	10	10	10
Total anaerobic phase (min)	90	90	120	120
Aerobic phase (min)	155	205	205	195-205
Anoxic phase (min)	50	30	0	0
Settling (min)	15	15	15	15-25
Effluent withdrawal (min)	10	10	10	10
Total cycle time (min)	360	360	360	360
Feeding time (min)	10±4	49±19	22±8	41±13
FT/TT* (%)	4±1	16±3	6±2	13±4

\*FT/TT: anaerobic mixed feeding time to total cycle time ratio

147 For both reactors, a relatively constant F/M ratio of 0.15kgCOD.(kgMLSS.day)<sup>-1</sup> was applied  
 148 by adjusting the feeding time with respect to the influent COD concentration and the MLSS  
 149 concentration. As a result the ratio of the SBR anaerobic mixed feeding time to the total cycle  
 150 time (FT/TT) varied during the experiment. For both lab-scale experiments, the DO  
 151 concentration was maintained between 1.0-1.5mgO<sub>2</sub>.L<sup>-1</sup> using an on/off aeration control  
 152 strategy and no pH control was applied. For SBR<sub>M</sub> and SBR<sub>B</sub>, the sludge retention time was  
 153 kept constant at 43 and 63 days by the automatic removal of 353mL and 380mL, respectively,  
 154 of the sludge mixture during effluent withdrawal.

### 155 **Sludge characteristics and sludge staining**

156 All sludge samples used for analyses were taken at the end of the anoxic (SBR<sub>M</sub>) or aerobic  
 157 (SBR<sub>B</sub>) cycle phase. The MLSS concentration was measured by filtering 5mL of  
 158 homogeneous sludge mixture over a glass microfibre filter which was subsequently washed  
 159 with demineralized water and dried for 24h at 105°C. The sludge volume (SV) was  
 160 determined as described by APHA/AWWA/WEF (1998). The median particle size  
 161 distribution by volume, DV<sub>50</sub>, was measured using a Malvern Mastersizer 3000 (Malvern,  
 162 UK) as described by Stes et al. (2018). Weekly analysis of the sludge was performed to  
 163 investigate the evolution of the sludge morphology using a CX21FS2 Olympus microscope.  
 164 Gram (modified Hucker method) and Neisser staining's were performed according to the  
 165 methods described by Jenkins et al. (2004) in the attempt to identify specific filamentous  
 166 organisms present in the system.

### 167 **Microbial community composition by 16S rRNA gene amplicon sequencing**

168 Genomic DNA was purified according to the NaTCA method (McIllroy et al. 2008) from  
 169 sludge samples taken in triplicate from the reactor on regular time intervals. A sequencing  
 170 library pool targeting the V1-3 region of the 16S rRNA gene was generated as described by  
 171 Karst et al. (2016), with minor modifications. Briefly, Phusion High-Fidelity DNA  
 172 polymerase (Thermo Scientific) and barcoded primers (IDT) were used for library PCR with  
 173 10-20ng of DNA as template and the denaturation step was carried out at 98°C. The resulting

174 library pool was submitted to a final purification step by gel extraction using NucleoSpin Gel  
175 and PCR Clean-up (Macherey Nagel), and diluted to obtain a 4 nM library pool. Amplicon  
176 sequencing was carried out on a Illumina Miseq system at the Centre for Medical Genetics  
177 (Edegem, Belgium) with the MiSeq Reagent Kit v3 (Illumina). The obtained paired-end reads  
178 were processed with the UPARSE pipeline (Edgar et al. 2013). As a reference database for  
179 taxonomy prediction, MiDAS (version 2.1) was used, which is a manually curated SILVA  
180 16S rRNA taxonomy (release 1.23 Ref NR99) that proposes a name for all the abundant  
181 phylum- and genus-level taxa present in activated sludge, anaerobic digesters and influent  
182 wastewater (McIlroy et al. 2015).

### 183 **In-situ cycle measurements during SBR operation**

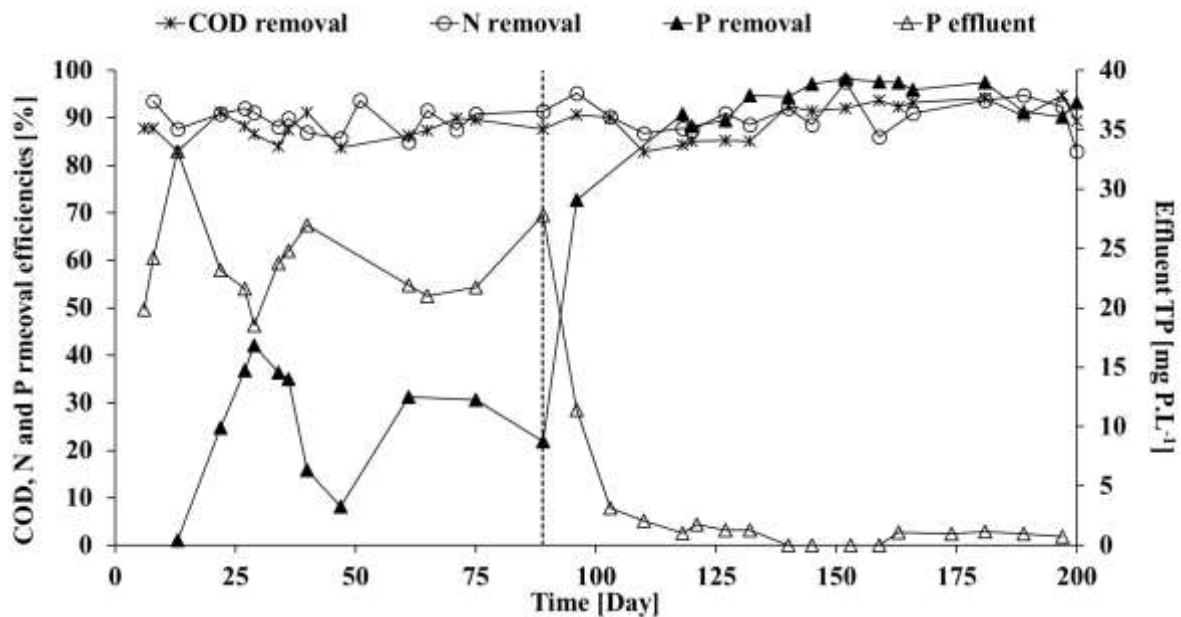
184 Due to the SBR operational strategy and subsequently the presence of granule structures, the  
185 enrichment of GAO/PAO like organisms is expected. In-situ cycle measurements during SBR  
186 operation are performed to determine the anaerobic carbon uptake and the degree of anaerobic  
187 phosphorus release and the aerobic phosphorus uptake rate. This was done to investigate the  
188 impact of the feeding rate on the GAO/PAO competition, favoring PAOs when the feeding  
189 rate was lowered. To determine the carbon and phosphate profiles, grab samples were taken  
190 (1) before and (2) after feed, (3) before aeration, (4) during aeration and (5) at the end of the  
191 SBR cycle. Grab samples were filtered immediately followed by the analytical measurements.  
192 From these results, the anaerobic carbon uptake [%], anaerobic P release [ $\text{mg P.g MLSS}^{-1}$ ]  
193 and aerobic P uptake rates [ $\text{mg P (g MLSS.h)}^{-1}$ ] were calculated.

## 194 **Results and Discussion**

### 195 **Low COD/P malting wastewater**

#### 196 **Reactor performance**

197 The feed to mass ratio (F/M) was kept relatively constant by adjusting the feeding volume  
198 in function of the influent COD concentration and the MLSS concentration. For SBR<sub>M</sub> the  
199 average F/M ratio was  $0.15 \pm 0.03 \text{ kg COD. (kg MLSS.day)}^{-1}$ . Due to changes in MLSS  
200 concentration and the aim to work at a constant F/M ratio, the organic loading rate (OLR)  
201 varied strongly with an average OLR of  $0.99 \pm 0.43 \text{ kg COD. (m}^3 \cdot \text{day)}^{-1}$ . To investigate the  
202 influence of the anaerobic feeding rate on the sludge characteristics and metabolic processes  
203 associated with the presence of slow-growing organisms, the feeding rate was lowered  
204 resulting in an increase of the average anaerobic mixed feeding time from  $10 \pm 4 \text{ min}$  up to  
205  $49 \pm 19 \text{ min}$ . This adjustment in feeding regime implicates a lower in-reactor substrate  
206 concentration during the anaerobic mixed feeding phase. The average OLR<sub>feeding</sub> was  
207  $0.69 \pm 0.18$  and  $0.34 \pm 0.09 \text{ kgCOD(m}^3 \cdot \text{h)}^{-1}$  during period I and II, respectively.



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**Figure 1** Evolution of the COD, nitrogen and phosphorus removal efficiencies and effluent phosphorus concentrations for SBR<sub>M</sub> (dotted line: introduction of prolonged feeding phase)

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The COD, N and P removal efficiencies were calculated for both operational periods showing stable carbon and nitrogen removal efficiencies throughout the experiment. Nitrogen removal was obtained through the two-step nitrification/denitrification process showing high removal efficiencies during the complete experiment. Effluent total nitrogen (TN) concentrations were consistently below 15mg N.L<sup>-1</sup> (Belgian discharge limit) with NO<sub>3</sub><sup>-</sup> as the main effluent nitrogen compound with a maximum concentration of 5.1mg NO<sub>3</sub><sup>-</sup>-N.L<sup>-1</sup>. Introduction of the prolonged feeding strategy did not have any impact on the N removal process. However, the adjustment of the feeding pattern had a major impact on the P removal efficiency due to the rapid increase of bio-P activity during period II. As can be seen in **Figure 1**, high effluent phosphate concentrations (>20mg PO<sub>4</sub><sup>3-</sup>-P.L<sup>-1</sup>) were measured during period I while during period II the effluent phosphate concentrations were consistently below 2mg PO<sub>4</sub><sup>3-</sup>-P.L<sup>-1</sup>. The average P removal efficiency was 26±13% during period I which is remarkably low compared to 89±8% during period II. For SBR<sub>M</sub> the pH varied between 6.8-7.2 within the anaerobic phase so it was assumed that phosphorus removal may not occur during operation of SBR<sub>M</sub>, especially during period I (short feeding time) due to the competitive advantage for anaerobic carbon uptake by GAOs. The results considering the absence of bio-P activity during period I confirm the findings by Filipe et al. (2001a) that GAOs show a competitive advantage for anaerobic carbon uptake when pH values are below 7.25. Additionally, the strong increase of bio-P removal when the anaerobic mixed feeding was prolonged is in line with results described by Tu et al (2013). They found that lowering the feeding rate in a lab-scale SBR fed with synthetic wastewater led to a shift in the GAO/PAO competition, favouring PAOs over GAOs even when pH is below 7.2. This was explained by the fact that PAOs contain an additional energy source for anaerobic carbon uptake, i.e. internally stored poly-P. Our results seem to confirm the statement made by Liu et al. (1997) that the PAO/GAO competition is an energy based competition for anaerobic carbon uptake which tends to favour poly-P containing PAOs over GAOs when in-reactor substrate concentration are low. To gain more insight in the shift in metabolic processes



238 occurring within the system, carbon and phosphate concentrations were profiled by the use of  
239 in-situ cycle measurements.

#### 240 **In-situ cycle measurements**

241 In-situ cycle measurements were performed showing minor anaerobic phosphate release  
242 during period I while anaerobic COD uptake from 74 up to 94% was observed. Together with  
243 the sludge settling characteristics and morphology (see further), the results indicate the  
244 presence of GAO like organisms in the system during period I. This is in line with previous  
245 findings described by Filipe et al. (2001a) showing that when pH is below 7.25, GAOs tend to  
246 be more dominant when a mixed anaerobic pulse feed is applied. During period II, anaerobic  
247 carbon uptake varied between 74% and 89% while a drastic increase of the anaerobic P-  
248 release and aerobic P-uptake rates was observed, as can be seen in **Table 3**.

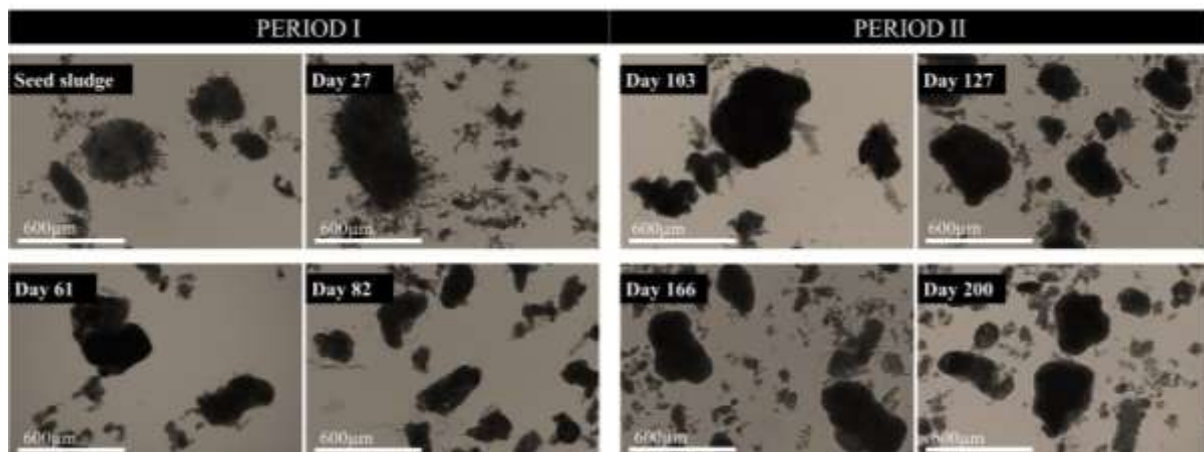
249 **Table 3** Evolution of the anaerobic P-release and aerobic P-uptake rate for SBR<sub>M</sub>

	Day	Anaerobic P-release [mg P.(g MLSS) <sup>-1</sup> ]	Aerobic P-uptake rate [mg P.(g MLSS.h) <sup>-1</sup> ]
Period I	6	1.19	0.36
	20	0.61	0.41
	34	1.27	0.60
Period II	96	6.12	3.16
	159	5.99	9.42
	196	5.71	5.70

250 Together with the increased phosphorus removal efficiencies up to 98%, it can be concluded  
251 that lowering the feeding rate has induced the enrichment of PAOs over GAOs in the system.  
252 Our results confirm the findings of Tu & Schuller (2003) that applying a low feeding rate  
253 promotes bio-P activity and seems to be more critical than the pH. This is, to our knowledge,  
254 the first time that the influence of the feeding time on the bio-P activity is investigated while  
255 treating an industrial wastewater in a C-SBR.

#### 256 **Granule characteristics**

257 Evolution of the granule settling characteristics, DV<sub>50</sub> and sludge morphology were  
258 investigated to determine the influence of the feeding regime on the overall granulation state  
259 and stability. During the first period of the experiment, the settling characteristics showed SVI  
260 values below 30mL.g<sup>-1</sup>. In addition, the average DV<sub>50</sub> was 209±3µm suggesting good  
261 selection for granule forming organisms. Meanwhile, filamentous outgrowth at the granule  
262 surface gradually decreased.



263

**Figure 2** Overview of the sludge morphology for SBR<sub>M</sub> during Period I and period II

264 Granule settleability only slightly decreased during period II, resulting in final SVI<sub>10</sub> and  
 265 SVI<sub>30</sub> values of 78mL.g<sup>-1</sup> and 47mL.g<sup>-1</sup>, respectively on day 200 of the experiment. These are  
 266 still considered as values representing good settling granular sludge. Lowering the anaerobic  
 267 feeding rate did not influence the overall granule morphology as shown in **Figure 2**.

268 However, it can be observed that smaller granular structures developed during period II. The  
 269 final DV<sub>50</sub> was only 153±1µm on day 189. This phenomenon can be explained by the fact that  
 270 lower in-reactor substrate concentrations may lead to substrate diffusion limitations and  
 271 subsequently the development of smaller but still compact granule structures. It can be  
 272 concluded that lowering the feeding rate from 10±4min to 49±19min had no major impact on  
 273 the granule settling or morphological characteristics. However, the feeding rate had a major  
 274 impact on the reactor performance considering the increased bio-P activity during period II of  
 275 the experiment. These results point out that applying a low anaerobic mixed feeding rate may  
 276 be a easily applicable operational strategy to promote biological phosphorus removal in an  
 277 AGS system for the treatment of malting wastewater in a compact C-SBR. Considering all  
 278 results, a low in-reactor substrate concentration is thought to select for (smaller) PAO like  
 279 granules over GAO which is assumed to be due to the presence of an additional energy  
 280 source, i.e. poly-P, for anaerobic carbon uptake. This, however, raises some questions  
 281 concerning the applicability of a low feeding rate for the treatment of wastewaters without  
 282 excess phosphorus, like brewery wastewater.

### 283 **High COD/P brewery wastewater**

#### 284 **Reactor performances**

285 For this experiment, a lab-scale SBR<sub>B</sub> treating brewery wastewater was operated for  
 286 approx. 400 days, divided into two periods based on the anaerobic mixed feeding rate. The  
 287 average F/M ratio and OLR were 0.20±0.09kg COD.(kg MLSS.day)<sup>-1</sup> and 0.93±0.42kg  
 288 COD.(m<sup>3</sup>.day)<sup>-1</sup>, respectively. On day 182 the mixed feeding rate was decreased resulting in  
 289 an increase of the average feeding time from 22±8min during period I up to 41±13min during  
 290 period II. Consequently, the average OLR<sub>feeding</sub> decreased from 0.78±0.18 to 0.25±0.07kg  
 291 COD.(m<sup>3</sup>.h)<sup>-1</sup>. Stable COD, N and P removal efficiencies of 98±1%, 99±1 and 96±4%,  
 292 respectively, were obtained throughout the experiment. When comparing period I and II, the  
 293 overall removal efficiencies were stable and the differences between both periods were found  
 294 to be negligible.

295

#### 296 **In-situ cycle measurements**

297 Throughout the experiment, in-situ cycle measurements were performed to evaluate the  
 298 influence of the feeding rate on the bio-P activity, i.e. the anaerobic P release and the aerobic  
 299 P uptake rate. When treating brewery wastewater the in-reactor pH is expected to be above  
 300 7.25 promoting minor bio-P activity as described by Stes et al. (2018). Since the pH is known  
 301 to play a key role in the competitions between GAO/PAO (Filipe et al. 2001b), this parameter  
 302 was taken into account during the study. The average pH was  $8.1 \pm 0.1$  which is generally  
 303 known to favour PAOs over GAOs. As can be seen in **Table 4** an increase of the anaerobic P-  
 304 release was observed during period I. These results suggest that even though the COD/P ratio  
 305 of the influent was high, minor enrichment of some granule forming PAO like organisms may  
 306 have occurred during period I. These findings are in line with the results reported by Stes et  
 307 al. (2018) where stable aerobic granules showed minor bio-P activity when the  $\text{pH} > 7.2$  while  
 308 treating brewery wastewater. Due to the alkaline conditions it is believed an additional energy  
 309 source is required to overcome the pH gradient across the cell membrane in order to take up  
 310 carbon anaerobically. Since PAOs can provide this additional energy requirement through  
 311 poly-P degradation, they tend to have a competitive advantage over GAOs (Filipe et al.  
 312 2001a). It is clear that the in-reactor pH can not be neglected in an anaerobic-aerobic operated  
 313 SBR system.

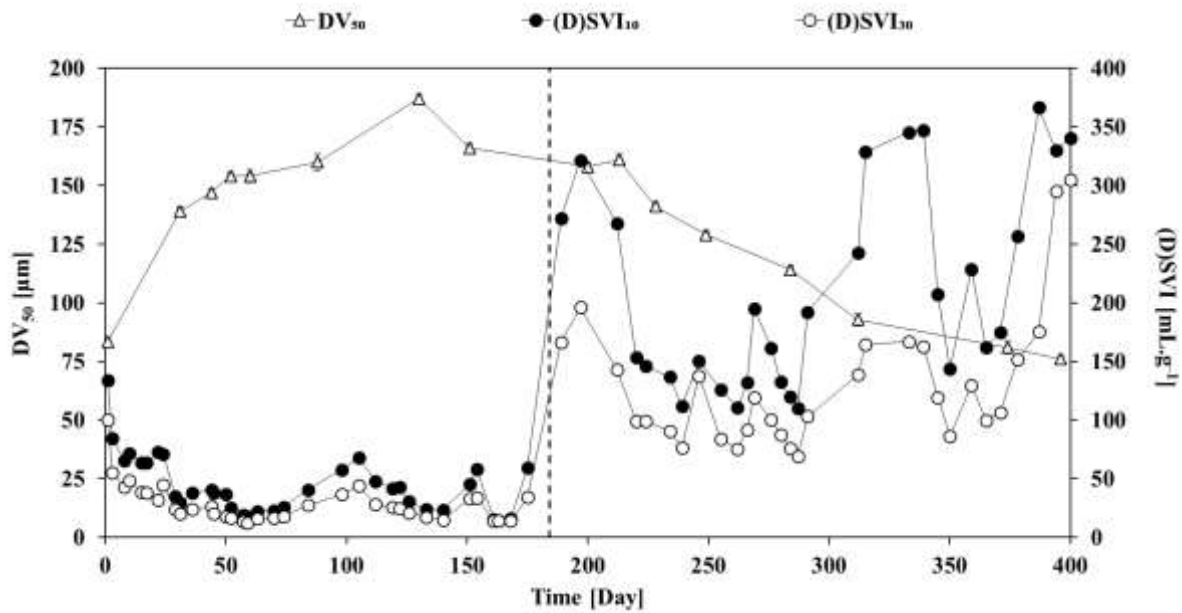
314 **Table 4** Evolution of the anaerobic P-release and the aerobic P-uptake rate for SBR<sub>B</sub>

	Day	Influent COD/P [%]	Anaerobic P release [mg P.g MLSS <sup>-1</sup> ]	Aerobic P-uptake rate [mg P.g MLSS <sup>-1</sup> ]
Period I	8	117	0.29	0.20
	15	189	0.47	0.36
	29	109	0.36	0.17
	34	138	0.15	0.08
	43	138	0.20	0.13
	57	135	0.38	0.15
	119	204	1.48	-
	142	92	1.68	0.37
	162	195	2.79	1.26
	182	126	3.15	2.54
Period II	211	270	1.34	1.98
	247	226	3.39	-
	283	370	1.49	1.98
	289	199	2.14	1.80
	379	222	1.50	1.67
	393	177	0.88	1.87
	400	190	1.88	2.48

315 In addition, results show that anaerobic P release as well as the aerobic P-uptake rates are  
 316 somewhat higher during period II compared to period I. These results illustrate that when  
 317 treating brewery wastewater with a high COD/P ratio, the anaerobic mixed feeding rate has  
 318 no significant influence on the bio-P activity. These findings are less clear compared to those  
 319 in SBR<sub>M</sub> which showed a strong increase in the bio-P activity when the feeding rate was  
 320 decreased. It is suggested that during this experiment, next to the pH and the feeding rate, the  
 321 high COD/P ratio had a major contribution on the competition between GAO and PAO like  
 322 organisms, possibly preventing PAOs to proliferate.

323 **Sludge characteristics**

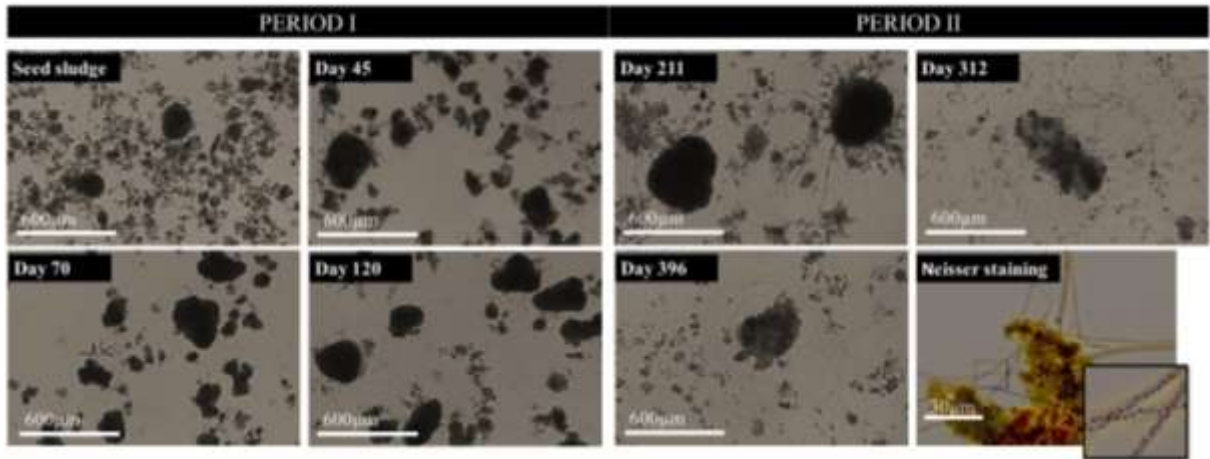
324 The evolution in granule settleability, granular size and morphology were investigated to  
 325 determine the influence of the feeding regime on granule characteristics and stability when  
 326 treating brewery wastewater. When comparing the sludge settling characteristics, results show  
 327 a significant difference between the two operational periods. **Figure 3** shows the evolution of  
 328 the DV<sub>50</sub> and (D)SVI values during the 400 days of operation.



329  
 330 **Figure 3** Evolution of DV<sub>50</sub> and (D)SVI<sub>10,30</sub> for SBR<sub>B</sub>. (dotted line: introduction of prolonged feeding time)

331 When comparing the (D)SVI values it is clear that selection of well settling sludge was  
 332 established during period I resulting in a decrease in (D)SVI values below 50mL.g<sup>-1</sup>. The  
 333 prolonged mixed feeding strategy was introduced on day 184. Hereafter, the (D)SVI<sub>10</sub> values  
 334 increased strongly up to 322mL.g<sup>-1</sup> on day 197. Subsequently, the settling characteristics  
 335 drastically deteriorated often resulting in very high SVI<sub>30</sub> values above 200mL.g<sup>-1</sup> during  
 336 period II. It is clear that increasing the FT/TT ratio had a major negative impact on sludge  
 337 settleability when treating brewery wastewater. Additionally, it became clear that during  
 338 period II the settling characteristics deteriorated rapidly when the difference between the  
 339 influent COD<sub>t</sub> and COD<sub>s</sub> concentration, i.e. ΔCOD, increased (data not shown). This is in line  
 340 with findings reported by de Kreuk et al. (2010) that the presence of particulate matter in the  
 341 influent has a negative influence on the overall AGS characteristics. However, the increase of  
 342 influent ΔCOD had a greater impact on the settling characteristics during period II compared  
 343 to period I. This suggests that lowering the feeding rate and thus the in-reactor substrate  
 344 concentration had a negative impact on the overall stability of the sludge settleability. In Stes  
 345 et al. (2018) successful aerobic granulation in an SBR treating brewery wastewater was  
 346 reported showing very low SVI<sub>30</sub> values (<50 mL.g<sup>-1</sup>). They applied a non-mixed (static)  
 347 pulse feeding strategy to obtain a maximum substrate concentration during the subsequent  
 348 anaerobic mixed feast phase. The brewery wastewater used by Stes et al. (2018) was also  
 349 characterised by strong fluctuations of the particulate matter content but showed no  
 350 significant effect on the sludge settling characteristics. It is clear that an high substrate  
 351 gradient during the anaerobic feast phase had a positive impact on the sludge settling  
 352 characteristics and the stability of the system towards variations in influent composition.

353 Evolution of the sludge morphology was investigated by microscopic analysis and shown in  
354 **Figure 4**.



355  
356 **Figure 4** Evolution of the sludge morphology during period I and II from SBR<sub>B</sub> (incl. example of a Neisser  
357 sludge sample).

358 It can be concluded that during period I dense granular structures developed and only a  
359 limited amount of filamentous organisms were present. Preservation of the large granules  
360 within the system was successful throughout period I. The morphology during period I is in  
361 strong contrast with period II where less dense, medium large granule structures, small flocs  
362 and filamentous organisms dominated the overall sludge morphology. These observations  
363 indicate that the increase of the (D)SVI values during period II are caused by the increased  
364 presence of smaller flocs and filamentous structures. In the attempt to identify the filamentous  
365 organisms and to confirm the presence of poly-P activity, i.e. intracellular poly-P granules,  
366 Neisser staining's were performed. As previously discussed, the in-situ cycle measurements  
367 showed bio-P activity within the system which was relatively high during period II  
368 considering the high COD/P ratio. Sludge samples were taken at the end of the aerobic phase  
369 to insure a maximum poly-P content within the cells. Remarkably, no accumulation of poly-P  
370 was observed within the granular sludge structures while it was clearly present within the  
371 filamentous organisms (see **Figure 4**). Only a limited number of filamentous organisms are  
372 known to have the capacity to store poly-P granules. In addition, Gram-staining responses  
373 were positive for the filamentous structures (data not shown). Considering the SBR<sub>B</sub>  
374 operational strategy (anaerobic feast to promote carbon conversion into intracellular  
375 polymers) and based on the staining results and the filament morphological characteristics  
376 only two specific filamentous organisms are suggested to be present in SBR<sub>B</sub>, i.e. *Thiothrix*  
377 spp. or *M. parvicella* (Jenkins et al. 2004). Both species are known to be able to accumulate  
378 carbon intracellularly as poly-hydroxyalkanoates (PHA) and have the capacity store  
379 phosphorus intracellularly (Rosetti et al. 2005; Rubio-Rincón et al. 2017). Molecular analysis  
380 by 16S-rRNA gene amplicon sequencing was performed in order to gain insight in the overall  
381 biomass composition of the seed sludge (Sample 1) and additionally identify the filamentous  
382 organisms at the end of period II (Sample 2). In supplementary data III<sub>a-b</sub> a detailed overview  
383 of the microbial composition at different taxonomical levels can be found. For sample 1 and  
384 2, up to 97% and 93%, respectively, of the resulting sequences could be classified at phylum  
385 level and up to 62% and 68%, respectively, at genus level. For sample 1, Planctomycetes and  
386 Bacteroidetes were the most abundant phyla representing 30% and 25% of all bacteria,  
387 respectively. For sample 2, Proteobacteria and Bacteroidetes were the most abundant phyla

388 raching up to 45% and 39% of the bacteria, indicating a shift in microbial composition during  
389 this study. The read abundance for *C. Accumulibacter* (PAO), known as an anaerobic carbon  
390 storing organism associated with granule formation, slightly increased from  $0.00\pm 0.04\%$  in  
391 sample 1 up to  $0.14\pm 0.05\%$  in sample 2. For *Defluviicoccus* (GAO) the read abundance in the  
392 seed sludge was  $0.71\pm 0.07\%$  and  $0.76\pm 0.06\%$  at the end of period II. No enrichment of other  
393 known PAOs or GAOs was observed during this study (see supplementary data III<sub>c</sub> for the  
394 resulting read abundances for all known GAOs and PAOs). The suggestion, based on  
395 microscopic observations that *M. parvicella* may be present in the system was countered by  
396 the 16S rRNA amplicon sequencing analysis indicating the complete absence in both sludge  
397 samples. However, the presence and strong enrichment of the *Thiothrix* genus  
398 (Proteobacteria) was confirmed by 16S rRNA amplicon sequencing analysis with an average  
399 read abundance of  $0.0\pm 0.0\%$  in the seed sludge and  $7.25\pm 2.27\%$  at the end of period II. The  
400 enrichment of *Thiothrix* in an anaerobic-aerobic granular sludge system was also observed by  
401 Stes et al. (2018) treating brewery wastewater in an anaerobically fed SBR. Since the  
402 presence of sulphur compounds was not taken into account during this study, measurements  
403 of the influent sulphate concentrations are absent. However, the anaerobic feeding strategy  
404 and the enrichment of *Rhodobacter* (Proteobacteria), known as a sulphate reducing organism,  
405 indicate the presence of sulphur compounds in the brewery wastewater. The read abundance  
406 for *Rhodobacter* increased from  $0.28\pm 0.03\%$  in sample 1 up to  $1.95\pm 0.28\%$  in sample 2. By  
407 applying a prolonged anaerobic phase, sulphate reduction was found to be promoted and  
408 subsequently to induce growth of filamentous sulphur bacteria in an anaerobic/aerobic SBR  
409 system (Baetens et al. 2001). It is likely that enrichment of *Thiothrix* spp. was promoted by  
410 the prolonged anaerobic SBR phase which was applied to promote anaerobic carbon uptake.  
411 Rubio-Rincón et al. (2017) showed that, in the presence of sulphide, *Thiothrix caldifontis* has  
412 the capacity to store carbon anaerobically as intracellular polymers and contribute to bio-P  
413 removal using stored poly-S as an additional energy source. These findings may explain our  
414 observations showing enrichment of poly-P storing filamentous organisms, i.e. *Thiothrix*,  
415 when applying an anaerobic/aerobic SBR operational strategy for the treatment of brewery  
416 wastewater. Although, minor filamentous outgrowth was observed during period I of the  
417 experiment suggesting growth of granule forming organisms is promoted over filamentous  
418 organisms during period I. It is suggested that, like *M. parvicella*, other filamentous carbon  
419 storing organisms show a higher substrate affinity compared to granule forming organisms  
420 when in-reactor concentrations are low during anaerobic mixed feeding. It is expected that  
421 sulphur compounds were present in the brewery wastewater. This complements the  
422 explanation to why more filamentous outgrowth, i.e. *Thiothrix*, was observed during period II  
423 compared to period I due to an increased energy demand for anaerobic carbon uptake when  
424 in-reactor substrate concentrations decline.

## 425 **Summary and conclusion**

426 The aim of this study was to investigate the influence of the anaerobic mixed feeding rate on  
427 the aerobic granule stability, reactor performance and bio-P activity while treating an  
428 industrial wastewater with a relatively low (malting) and high (brewery) COD/P ratio. In both  
429 cases, selection of carbon storing organisms was promoted by applying a feast/famine regime  
430 through anaerobic/aerobic/anoxic SBR cycle operation. It can be concluded that for SBR<sub>M</sub> a  
431 decrease of the  $OLR_{\text{feeding}}$  resulted in a strong increase in bio-P activity and is therefore  
432 assumed to promote growth of PAO over GAO. The effect on the granule settleability was  
433 only minor and dense granular structures were preserved. This is to our knowledge the first  
434 time that the positive effect of a prolonged feeding time on the bio-P removal activity in an

435 AGS system is investigated while treating an industrial wastewater in a C-SBR. When  
436 treating brewery wastewater characterised by a high COD/P ratio, successful granule  
437 formation was achieved by applying an anaerobic mixed pulse feeding strategy. Sludge  
438 morphology was dominated by dense granule structures showing good and stable settling  
439 characteristics suggesting successful selection for granule forming organisms. A decrease of  
440 the anaerobic mixed feeding rate resulted in deterioration of the granular sludge combined  
441 with filamentous outgrowth. In-situ cycle measurements showed no increase in bio-P activity  
442 while Neisser staining showed intracellular poly-P granules within filamentous organisms.  
443 This shift in sludge morphology towards enrichment of filamentous organisms had a negative  
444 impact on the settleability of the biomass. It is suggested that the high influent COD/P ratio  
445 prevented proliferation of PAO like organisms within the system promoting enrichment of  
446 high affinity filaments over granule forming groups. Through this study, the importance of the  
447 anaerobic mixed feeding rate in a C-SBR system is confirmed. When considering application  
448 of the AGS technology in conventional mixed SBR systems, the anaerobic mixed feeding rate  
449 should be taken into account. In this study, a new operational parameter,  $OLR_{\text{feeding}}$ , was  
450 defined to allow quantification of the feeding rate from a substrate loading point of view.

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