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Experimental investigation of methane hydrate formation in the presence of metallic packing

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ABSTRACT

Clathrate hydrates gained significant attention as a viable option for large-scale storage of natural gas, primarily methane (CH₄). Unlike employing the nanoconfinement for enhancing the nucleation sites and hydrate growth as in the porous materials, whose synthesis is often associated with high costs and poor batch reproducibility, a new approach for promoting CH₄ hydrates using pure water (H₂O) in an unstirred reactor packed with stainless steel beads (SSB) was proposed in this fundamental work, where the interstitial space between the beads was exploited for enhanced hydrate growth. SSB of two diameters, 5 mm and 2 mm, were used as

20 a packed bed to investigate their effects on CH₄ hydrate formation at 273.65 K, 275.65 K, and
21 277.65 K with an initial pressure of 6 MPa. The thermal conductivity of SSB packing
22 potentially aided hydrate growth by expelling the hydration heat, while, the results also
23 revealed that driving force has a substantial impact on the rate of CH₄ hydrate formation and
24 gas uptake. The experiments conducted in both 5 mm and 2 mm SSB packed bed reactors
25 showed a maximum gas uptake of 0.147 mol CH₄/mol H₂O at 273.65 K with water to hydrate
26 conversion of 84.42% with no significant variation. The results established the promotion
27 effect on the kinetics of CH₄ hydrate formation in the unstirred reactor packed with 2 mm SSB
28 due to the availability of more interstitial space offering multiple nucleation sites for CH₄
29 hydrate by providing a larger specific surface area for H₂O-CH₄ reaction. Experiments with
30 varying H₂O content were also performed and the results showed that the water to hydrate
31 conversion and rate of hydrate formation could be enhanced at a lower H₂O content in a packed
32 bed reactor. This study demonstrates that the use of costly or intricate porous materials can be
33 made redundant, by exploiting the interstitial voids in packing of cheap and widely available
34 SSB as a promising alternative material for enhancing the kinetics of artificial CH₄ hydrate
35 synthesis.

36 **KEYWORDS:** methane hydrate, gas hydrates, hydrate formation, gas storage, fixed bed,
37 energy storage

38

39 1. Introduction

40 The demand for basic energy sources such as coal, oil, natural gas is increasing as a result of
41 rapid growth in population, industrial advancement, and transportation. The large depletion of
42 coal and oil reserves and carbon dioxide emissions associated with their use has shifted the
43 attention of governments and their energy policies towards utilizing natural gas and hydrogen
44 as an imperative condition for global environmental security[1-6]. Natural gas which is > 95

45 percent methane (CH₄), has been touted as an excellent alternative to coal and oil as a fuel for
46 power generations and transportation due to its low carbon emission characteristics such as
47 releasing considerably lesser degree of pollutants upon combustion per energy basis[7, 8].

48 Despite CH₄ being acknowledged as a potential energy source[9], the major challenge is in
49 its handling, and achieving high storage capacities both economically and safely. The
50 commercially available methods like liquified natural gas (LNG) and compressed natural gas
51 (CNG), which are capable of achieving predominant volumetric capacities (≈ 600 v/v for LNG,
52 ≈ 240 v/v for CNG) and energy densities (22.2 MJ/l for LNG and 9 MJ/l for CNG[10]) greatly
53 suffer from their expensive cryogenic (113 K) and high-pressure (25 MPa) storage approaches
54 that prevent their widespread use[11-15]. In this light, another promising alternative technology
55 that gained significant attention for potential natural gas storage and transportation is the
56 formation of natural gas hydrates (NGHs)[16-19] and a comprehensive review of
57 advancements in gas hydrates research on challenges, limitations, and future perspective is
58 presented by Hassanpouryouzband et al.[20]. Gas hydrates or clathrate hydrates are
59 nonstoichiometric crystalline compounds that form at high pressures and low temperatures
60 when suitable sized gas molecules (CH₄ in this work; guest) are trapped in the cage structures
61 built by the hydrogen-bonded water (H₂O) molecules (host), where the trapped CH₄ molecules
62 stabilize the H₂O lattice via van der Waals forces[2, 21]. NGHs, primarily CH₄ hydrates can
63 deliver approximately 170 m³ of CH₄ gas per unit volume at moderate storage conditions[2,
64 22, 23]. Alongside storage capacity, they are also considered safe because of their non-
65 explosive nature and cost-effectiveness compared to the commercial methods[24-27], but it is
66 also important to emphasize that gas leaks from clathrates can be unsafe in case of improper
67 storage and transport conditions. In addition to their natural gas storage application, hydrates
68 can be used for the capture of CO₂ from flue gases[28, 29], gas separation[30], refrigerants[31],
69 hydrogen storage[6], and water desalination[32]. However, the gas hydrate technology is not

70 yet industrially competitive with the existing storage and transport methods and is critically
71 challenged due to its low water-to-hydrate conversion, slow formation kinetics, and extremely
72 low temperatures to keep them stable at atmospheric pressure[33]. Most of these challenges
73 are caused by inadequate contact between gas/water (mass transfer) and the generation of large
74 hydrate heat which does not promote hydrate formation and growth[34]. Consequently,
75 enhancing the mass transfer and heat transfer by effective gas/water contact and removing the
76 hydration heat respectively are necessary for an efficient hydration process.

77 Tremendous research has been focused on overcoming the above-mentioned challenges by
78 employing mechanical methods such as stirring[35-44], gas bubbling[45-47], and spraying[48-
79 51], however, some drawbacks associated with these approaches hinder them for practical
80 applications. Mechanical agitation in a stirred tank reactor is a matured and conventional
81 technique. Despite advantages such as shorter induction times and faster hydrate formation
82 rates at early stages[52], stirred tank reactors have a disadvantage of limited conversion of
83 water and gas to hydrates due to agglomeration of hydrate crystals; acting as a barrier that
84 prevents efficient contact between gas and liquid[53, 54]. Other disadvantages are the
85 decomposition of hydrates over long-term stirring[42], the high energy cost for stirring upon
86 thickening of hydrate slurry[35, 45], and inconvenience in separating the produced hydrates on
87 a continuous production scale[55]. Besides mechanical stirring, the major underlying problem
88 in spray reactors is the ineffective cooling upon hydrate formation[56]. Another alternative
89 approach is the use of bubble tower reactors that have the advantage of better contact between
90 gas and liquid, at the same time suffer from disadvantages like separation of formed hydrate at
91 the gas/liquid interface and limited heat transfer rates during hydrate formation[45]. Though
92 the rate of hydrate formation is high on a fresh bubble, the hydrate shells at a later stage were
93 found to agglomerate rather than merging into bigger bubbles and hindering further hydrate

94 formation. A comprehensive review on reactor design and their associated challenges upon
95 scaling up is presented by A. Gupta et al.[6] and Y. H. Mori[57].

96 Aside from new reactor designs, continuous research efforts have been communicated[9, 58-
97 75] in enhancing the kinetics of CH₄ hydrate formation by the use of thermodynamic promoters
98 or kinetic promoters (predominantly surfactants), where these surfactants reduce the interfacial
99 tension between (guest) gas-liquid (host) interface and enhance the hydrate growth (mass
100 transfer of gas and liquid phase) without affecting the thermodynamics[67, 68]. Nevertheless,
101 fast hydrate formation is always associated with high hydration heat which ultimately weakens
102 the acceleration effect of surfactants on hydrate formation[77, 78]. On the other hand, the
103 thermodynamic promoters which can alter the hydrate forming conditions, predominantly
104 occupy the larger cages of the hydrate and eventually lower the CH₄ storage capacity compared
105 to pure CH₄ hydrates, consequently a penalty on storage capacity is ineludible[71]. A
106 comprehensive list of both kinetic and thermodynamic promoters for CH₄ hydrates is presented
107 in our earlier publication[9].

108 Another alternative approach to enhance the kinetics of CH₄ hydrate formation rate is by
109 employing a fixed bed porous column without stirring and some of the existing research has
110 already shed light on suitable fixed bed packings to enhance water-to-hydrate conversion and
111 to boost the hydrate growth[25, 44, 76, 78-141]. Developing a synthetic porous material with
112 high storage capacity, high chemical, mechanical and thermal stability is assumed to be vital
113 for a successful and efficient storage process. Research is currently advancing in determining
114 such potential porous materials and some of them (including but not limited to) that are actively
115 pursued are carbon-based porous materials[25, 91, 142-144], silica-based materials[88, 94,
116 107, 141, 145-149], zeolites[122, 150-153], metal-organic frameworks[100, 120, 143, 154-
117 156]. Aside from the development of new synthetic methods, it is also important to mention
118 that mass production of these materials for large-scale applications is often associated with

119 high costs and poor reproducibility between batches[15, 157, 158]. Although a significant
120 amount of research has shown interest in the hydrate mass transfer rate, the constraints of heat
121 transfer have largely been overlooked although it plays a crucial role in potential scale-up. In
122 view of the latter, relatively limited studies[77, 159-174] have been conducted to enhance the
123 thermal conductivity of hydrate systems utilizing novel materials together with kinetic
124 promoters. More recently, open-cell aluminum metal, SiC foam with good thermal
125 conductivity was used to enhance the removal rate of hydration heat through the cell walls and
126 increase the CH₄ hydrate formation rate[76, 98, 175]. Similarly, stainless steel structured
127 packing in presence of a kinetic promoter was also used as a fixed-bed medium to enhance the
128 thermal conductivity of the bed for CO₂ hydrates[176].

129 Inspired by this, we used stainless steel beads (SSB) as a fixed-bed porous column for CH₄
130 enclathration in this study. Up till now, to our knowledge, there is no report in the literature
131 concerning how SSB packing affects the CH₄ hydrate formation and with this in mind, we
132 evaluate the effect of CH₄ hydrate formation kinetics in pure water at different temperatures
133 and constant pressure in presence of an SSB packed bed. Furthermore, the SSB packing can
134 enhance the thermal conductivity of the bed, concurrently, the thermal conductivity of stainless
135 steel beads ($\sim 14.6 \text{ W m}^{-1} \text{ K}^{-1}$)[177] being approximately 24 to 25 times higher than that of CH₄
136 hydrate ($\sim 0.60 \text{ W m}^{-1} \text{ K}^{-1}$)[178-180] can potentially accelerate hydrate growth by rapidly
137 removing the hydrate heat from the reaction. Accordingly, the kinetics of CH₄ hydrate
138 formation in presence of SSB packing, the effects of water content on gas uptake, and water to
139 hydrate conversions are also evaluated.

140 2. Experimental section

142 2.1 Experimental apparatus

143 As shown in Figure 1, the CH₄ hydrate formation experiments were carried out in cylindrical
144 stainless steel (SS) reactor (diameter: 48.3 mm, height: 20.3 mm, effective volume: 150 cm³)

145 purchased from Swagelok (316L-50DF4-150) with a pressure rating of 34.4 MPa. To obtain a
146 stable temperature and to control the temperature precisely, the SS reactor was immersed in a
147 high-precision circulating bath (CORIO CP-1000F, JULABO GmbH) filled with a water-
148 ethylene glycol mixture. The temperature stability of the bath was ± 0.03 K. The pressure
149 within the reactor was monitored by connecting a pressure transmitter (PAA3X-300bar;
150 KELLER AG; a range of 0-300 bar absolute) having an accuracy of $\pm 0.01\%$ FS. A data
151 acquisition system connected with a computer was used to record the temperature and pressure
152 every 1 second. Stainless steel beads of diameters 5 mm and 2 mm, purchased from IKATM
153 (Fisher Scientific platform) were used as the fixed-bed porous medium. Methane gas (99.99%
154 purity) used in this study was supplied by Air Liquide Benelux Industries and deionized water
155 with a resistivity of $18 \text{ m}\Omega\cdot\text{cm}^{-1}$ was made in the laboratory.

156 2.2 Experimental procedure

157 A standard approach was used to measure the formation of CH_4 hydrates at constant volume
158 and the experimental procedure may be described as follows. Prior to the experiments, the SS
159 316L reactor was cleaned with deionized water and dried with compressed air, followed by
160 packing the reactor with cleaned (with H_2O) and dried stainless-steel beads along with the
161 required volume of deionized water. Subsequently, the reactor was purged with CH_4 gas (0.2
162 MPa) 10 times to remove any residual air in the system. The reactor was then immersed in the
163 water-ethylene glycol bath (temperature: ~ 303 K) and CH_4 gas is injected slowly into the
164 reactor to a pressure of 6 MPa. Concurrently, the data acquisition started to record the bath
165 temperature and pressure inside the reactor at a 1 Hz frequency. The reactor was kept at this
166 steady ambient temperature to prevent any hydrate formation. After the temperature and
167 pressure being stabilized, the reactor was then cooled down to the experimental temperature,
168 and the time when these thermodynamic conditions, the temperature, and pressure of the
169 reactor reached the experimental conditions was considered as time zero. The hydrate

170 formation was considered to be complete when a pressure drop of less than 0.02 MPa in 30
 171 min was observed. It is also important to mention that the measurements were performed with
 172 an identical reference vessel (with SSB, but in absence of water) having the same configuration
 173 as the actual hydrate formation reactor (sample reactor). Each experiment was repeated two
 174 times. In this work, the amount of CH₄ gas consumed was used to determine the extent of CH₄
 175 hydrate formed. The dissolution of CH₄ gas was not considered in the current study due to its
 176 low solubility[141, 181] in water at these temperatures, and also the solubility of CH₄ being
 177 very small it can be neglected when compared to the amount of CH₄ consumed for hydrate
 178 formation. The gas consumption was calculated using the compressibility factor equation of
 179 state. The moles of CH₄ gas consumed during hydrate formation were calculated using (Eq. 1),

$$\Delta n_{hyd} = V_r \left(\frac{P_i}{Z_i RT} - \frac{P_t}{Z_t RT} \right) \quad (\text{Eq. 1})$$

180 where, Δn_{hyd} is the moles of CH₄ gas consumed at time t , V_r is the volume of gas-phase
 181 inside the reactor measured using helium expansion method[182, 183], P_i is the initial pressure
 182 of hydrate formation stage, P_t is the pressure of hydrate formation stage at time t in the reactor,
 183 R is the ideal gas constant, T is the temperature of the reactor, Z_i is the compressibility of gas
 184 at the start of hydrate formation and Z_t is compressibility factor of gas in the reactor at time t .
 185 The compressibility factors Z_i and Z_t are calculated using the Pitzer correlation[184]. The
 186 percentage of water to hydrate conversion ($C_{WH}(\text{mol } \%)$) is determined using (Eq. 2), and the
 187 normalized gas (NG_t) uptake at any given time t is calculated using (Eq. 3),

$$C_{WH}(\text{mol } \%) = \frac{\Delta n_{hyd} \times \text{hydration number}}{n_{H_2O}} \times 100 \quad (\text{Eq. 2})$$

188

$$NG_t = \frac{\Delta n_{hyd}}{n_{H_2O}} \quad (\text{mol of gas / mol of water}) \quad (\text{Eq. 3})$$

189

190 where, n_{H_2O} are the total number of moles of H₂O in the system and hydration number is
 191 defined as the number of H₂O molecules required to encapsulate one guest (CH₄) molecule,
 192 and the water-to-hydrate conversion in this work was calculated assuming the hydration
 193 number as 5.75[99, 133, 185]. A discrete first-order forward difference method was used to
 194 calculate the rate of CH₄ hydrate formation as shown in (Eq. 4), where Δt is the time difference
 195 between two observations.

$$\frac{dN_t}{dt} = \left(\frac{d\Delta n_{hyd}}{dt} \right) \approx \frac{\Delta n_{hyd,t+\Delta t} - \Delta n_{hyd,t}}{\Delta t}, \Delta t = 2 \text{ mins} \quad (\text{Eq. 4})$$

196
 197 Stainless steel beads (SSB) of diameters 5 mm and 2 mm were used as packing medium in
 198 the reactor to study the characteristics of the hydrate formation process. All the experiments
 199 were conducted by filling the reactor with 2.05 g H₂O and the experiments were carried out at
 200 an initial pressure of 6 MPa, and temperatures 273.65 K, 275.65 K, 277.65 K. As it is known
 201 that a larger driving force can favor (shorten) the hydrate formation induction time[36, 186] at
 202 a given temperature or pressure, this work sets the experimental pressure (P_{exp}) at 6 MPa. The
 203 CH₄ hydrate formation phase equilibrium curve from CSMHYD[187] and Kummamuru et
 204 al.[9] reports hydrate equilibrium pressure (P_{eq}) approximately at 2.7 MPa, 3.3 MPa, 4 MPa at
 205 273.65 K, 275.65 K, and 277.65 K respectively. Therefore, the driving force ($\Delta P = P_{exp} - P_{eq}$;
 206 at a given temperature) for hydrate formation in this work was calculated to be 3.3 MPa, 2.7
 207 MPa, and 2 MPa for the three selected temperatures, respectively.

208

209 3. Results and discussion

210 Table 1. summarizes the CH₄ hydrate experimental results from this work including
 211 maximum growth rate, water-to-hydrate conversion percentage at 273.65 K, 275.65 K, 277.65
 212 K in 5 mm and 2 mm SSB packed bed systems. Figure 2. shows the CH₄ uptake profile during
 213 hydrate formation in SSB (5 mm) packing at 273.65 K. An average gas uptake plot from three

214 experiments is shown along with the standard deviation and time zero corresponding to the
215 nucleation point for the experiment. As seen in the figure, a maximum uptake of 0.147 mol
216 CH₄/mol H₂O was achieved in 140 min, and as a comparison at these thermodynamic
217 conditions (273.65 K and 6 MPa), CH₄ gas solubility in H₂O is approximately 0.002 mol
218 CH₄/mol H₂O according to NIST database[188], indicating that it is fair to assume the gas
219 uptake is almost exclusively due to CH₄ enclathration in H₂O cages during hydrate formation.
220 SSB being non-porous, the possible explanation for CH₄ hydrate formation is the presence of
221 a higher driving force coupled with nucleation sites provided by the interstitial space between
222 SSB, which eventually promoted hydrate nucleation and aided further growth. Reports by Jin
223 et al.[189], Linga et al.[88] also support the current findings, where CH₄ hydrate has been
224 reported to form in the interstitial area between sand particles. Aside from providing nucleation
225 sites via interstitial space, the SSB packing may have also offered the service of rapid hydrate
226 heat transfer, which accelerated hydrate formation. Maximum water-to-hydrate conversion in
227 SSB (5 mm) packing and at these thermodynamic conditions was found to be approximately
228 84.4% in 140 min of hydrate growth. The inset in Figure 2. presents the gas uptake
229 measurements for the experiments conducted at 275.65 K and 277.65 K in a 5 mm SSB packed
230 bed filled with 2.05g H₂O. As can be seen, with an increase in temperature, the normalized gas
231 uptake decreased, where a maximum uptake of 0.137 mol CH₄/mol H₂O was achieved at
232 275.65 K in 525 min whereas it took approximately 3 times longer to reach a maximum gas
233 uptake of 0.094 CH₄/mol H₂O at 277.65 K compared to 275.65 K.

234 Figure 3. compares CH₄ hydrate growth rate in the 5 mm SSB packed bed at all the three
235 temperatures studied in this work for the first 140 min. An average gas uptake from three
236 experiments is shown along with the standard deviation and time zero corresponds to the
237 nucleation point for all of the experiments conducted. It can be seen that the rate of hydrate
238 formation increases as the temperature decreases, which clearly indicates the direct influence

239 of increased driving force. A maximum gas uptake of 0.069 mol CH₄/mol H₂O was achieved
240 at 275.65 K and 0.049 mol CH₄/mol H₂O at 277.65 K in 140 min, which is only 46.9% and
241 33% of the measured gas uptake at 273.65 K, respectively.

242 The effect of particle size on CH₄ hydrate formation was also investigated at the lowest
243 temperature of 273.65 K and 6 MPa by packing the reactor with 2 mm SSB. Figure 4. compares
244 the hydrate formation behavior in 5 mm and 2 mm SSB packing reactor filled with 2.05 g H₂O.
245 It can be observed that the experiments conducted with small SSB and large SSB, provide
246 almost identical maximal gas uptake values with no significant variation. However, it can be
247 deduced that the 2 mm SSB packing medium enhanced the rate of methane hydrate formation
248 due to the availability of more interstitial space (as a result of decreased beads size) which offer
249 multiple nucleation sites for CH₄ gas hydrate by providing a larger specific surface area relative
250 to 5 mm SSB packing which also improved the contact between gas-liquid-solid to be a priority
251 site for hydrate nucleation[125, 141, 190, 191]. Rapid hydrate growth is always associated with
252 the swift release of hydration heat. Aside from providing hydrate nucleation sites, the thermal
253 conductivity of 2 mm SSB packing may have enhanced hydrate formation by rapidly expelling
254 the hydration heat. A closer examination at the normalized gas uptake at the 10th min already
255 shows 0.119 mol CH₄/mol H₂O for 2 mm SSB packing, while 5 mm SSB packing at the same
256 time shows 70.58% lower uptake, reading 0.035 mol CH₄/mol H₂O.

257 Attempting to compare the performance of SSB packing with other reported packed bed
258 materials for promoting CH₄ hydrate formation could be of potential interest. However, merely
259 comparing the absolute values of hydrate growth rate, maximum stored capacity, water to
260 hydrate conversion drawn from various laboratories, methods and reactors may not be a reliable
261 way to determine which one leapfrogged the other. Such for instance, P. Hu et al.[115] and M.
262 Zi et al.[192] reported that any change in the microstructure of high-pressure metal made
263 reactor surfaces (roughness) would tremendously affect the hydrate growth rate which

264 subsequently affects water to hydrate conversion as well as induction time. In this regard, it is
265 also important to mention that most of the high-pressure reactors reported in the literature were
266 made of metal material. Furthermore, different experimental procedures can also have
267 significant effects on hydrate growth rate or induction time, for instance, in some of the
268 studies[115, 193] as well as in the present study, the hydrate forming gas (e.g. CH₄) was
269 introduced into the reactor before reaching the experimental temperature, contrarily, in other
270 studies[175, 194, 195], the hydrate forming gas is introduced into the reactor upon reacting the
271 experimental temperature. Compared with former conditions, both the hydrate gas dissolution
272 and nucleation may occur concurrently in latter conditions, which substantially narrows the
273 induction time. However, it is exemplary to make a comparison between the works using fixed
274 packing as the case in this study that has larger particle diameters providing nucleation sites
275 for hydrate formation. As shown in Figure 5, only the works[107, 141, 196-199] using fixed
276 packing materials having particle diameters greater than 1 mm were selected for comparison.
277 The results demonstrated that the water to hydrate conversion reported in previous studies
278 ranged from 16.8% to 84.43%, while the maximum water to hydrate conversion was upto
279 84.42% with 5 mm or 2 mm SSB packing employed in the present study. In comparison, the
280 water to hydrate conversion (84.43%) reported by Filarsky et al.[107] is relatively similar to
281 the conversion (84.2%) presented in this study, however, it is worth mentioning that the
282 experimental pressure employed in their study is two times higher than the pressure used in the
283 present work. In contrast to this work, it should also be emphasized that many of the studies
284 presented in Figure 5. used kinetic promoters to enhance the hydrate formation rate.

285 The rate of CH₄ hydrate formation in 5 mm SSB packing with the driving force of 3.3 MPa,
286 2.7 MPa, 2 MPa is presented in Figure 6. As can be seen, the rate of hydrate growth is higher
287 for the system with a larger driving force, followed by the other two driving forces in
288 decreasing order. For instance, at 2 min of hydrate growth, the rate is 3.28 times and 8.61 times

289 higher in the larger driving force (3.3 MPa) than in other driving force conditions 2.3 MPa and
290 2 MPa respectively. For the system with the larger driving force, the rate slows down and
291 reaches nearly zero in 140 min. Similarly, the rate of CH₄ hydrate formation in 2 mm SSB
292 packing and 5 mm SSB packing studies conducted at a driving force of 3.3 MPa are compared
293 in Figure 7. For smaller SSB packing, the rate of hydrate formation is relatively higher than the
294 larger SSB packing. In the first 10 min, a rapid hydrate rate can be observed in smaller SSB
295 packing followed by a gradual decrease and reaching zero in about 40 min indicating the
296 completion of hydrate formation, while the rate continues in larger SSB packing up till 140
297 min.

298 Additionally, the mass of H₂O in the reactor was varied and investigated to evaluate the
299 influence of H₂O content on hydrate formation. Figure 8. shows the gas uptake measurements
300 for the experiments conducted at 273.65 K and 275.65 K in a 5 mm SSB packed bed filled with
301 10.25 g H₂O and with an initial pressure of 6 MPa. As can be seen, the maximum gas uptake
302 achieved after 1794 min is 0.054 mol CH₄/mol H₂O at 273.65 K and 0.035 mol CH₄/mol H₂O
303 at 275.65 K. These results clearly show a decrease in gas uptake with an increase in H₂O
304 content from 2.05 g to 10.25 g. For instance, the gas uptake value for 10.25 g H₂O at the lowest
305 operating temperature in 5 mm SSB packing is 81.16% lower compared to that achieved with
306 2.05 g H₂O within the first 140 min. This infers that the rate of hydrate formation, water-to-
307 hydrate conversion could be accelerated when the water content is lower in a packed bed and
308 this is always relative to the amount of H₂O used[89, 132, 200]. Figure 9. compares the
309 normalized gas uptake measurements for the experiments conducted at 273.65 K and 275.65
310 K in a 5 mm SSB packed bed filled with 2.05 g and 10.25 g H₂O. It can be seen that experiments
311 performed with larger H₂O content were able to achieve approximately 30% of gas uptake at
312 similar thermodynamic conditions for lower H₂O content and the corresponding low rate of
313 hydrate formation can be seen in Figure S1. Comprehensively, this study highlights that SSB

314 packing can foster CH₄ hydrate formation at the thermodynamic pressures of 6 MPa and
315 temperatures over 273.15 K, as well as enhance hydrate growth at lower H₂O saturations by
316 altering the packing size.

317

318 4. Conclusion

319 The formation behavior of CH₄ hydrate in an unstirred reactor packed with different sizes of
320 stainless steel beads (SSB) was investigated in this study at three different temperatures of
321 273.65 K, 275.65 K, 277.65 K with a starting experimental pressure of 6 MPa. The results
322 demonstrated that both types of SSB employed in this study as the packing medium effectively
323 promoted hydrate formation and, in addition to offering nucleation sites, the thermal
324 conductivity of SSB conceivably favored by expelling the hydration heat. A maximum gas
325 uptake of 0.147 mol CH₄/mol H₂O was achieved at 273.65 K in 140 min in a 5 mm SSB packed
326 bed filled with 2.05 g H₂O. The experiments conducted at 273.65 K and 2.05 g H₂O in an
327 unstirred reactor packed with 2 mm SSB showed a higher rate compared to the reactor packed
328 with 5 mm SSB. However, the maximum water-to-hydrate conversion achieved in both
329 systems is similar, and approximately 84.42%. The smaller size SSB packing medium
330 effectively accelerated the CH₄ hydrate growth rate at an early stage due to the availability of
331 more interstitial space offering multiple nucleation sites for gas hydrate by providing a larger
332 specific surface area for water-gas reaction. A maximum gas uptake of 0.147 mol CH₄/mol
333 H₂O was achieved in 95 min which was approximately 45 min faster than for reaching a similar
334 gas uptake value in a 5 mm SSB packed bed reactor. This highlights the requirement for
335 optimizing the structure of the packed bed reactor to improve the contact between gas-liquid-
336 solid to be a priority site for hydrate nucleation. In addition, the influence of H₂O content on
337 hydrate formation was also evaluated in the 5 mm SSB packed bed reactor at 273.65 K and
338 275.65 K. The maximum water-to-hydrate conversion of 30.87% was achieved only after 1794

339 min of hydrate formation for 10.25 g of H₂O saturation at 273.65 K. In this vein, at a lower
340 H₂O saturation, it can be speculated that the surface contact area between the two phases (gas-
341 liquid) increased, resulting in rapid hydrate formation and gas consumption. Furthermore, it
342 can be deduced that tuning the H₂O saturation in a packed bed can maximize the rate of hydrate
343 formation and gas uptake. Conclusively, the results from this work could potentially eliminate
344 the porous material synthesis cost and the need for stirring, both of which are economically
345 beneficial, while also being a promising alternative material for enhancing CH₄ hydrate
346 synthesis in comparison to the extensive research on porous materials reported in the literature.
347 The findings from this work are also expected to be beneficial for large-scale natural gas
348 storage in the form of hydrates within a packed metal bed.

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358

359 **Notes**

360 The authors declare no competing financial interest.

361 **Supporting Information**

362 **The supporting information is available free of charge on the ACS Publications website**
363 **at DOI:**

364 Rate of CH₄ hydrate formation conducted at 273.65 K and 275.65 K in a 5 mm SSB packed
365 bed filled with 10.25 g H₂O

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868

Table 1. Summary of CH₄ hydrate formation at different experimental conditions in this study with P_{exp} of 6 MPa

System	T_{exp} (K)	Driving force (MPa)	end of experiment		NG_{t90} (mol CH ₄ /mol H ₂ O)	end of experiment	
			Time (min)	NG_t (mol CH ₄ /mol H ₂ O)		C_{WH} (mol%)	^a V_H (cm ³)
5 mm SSB	273.65	3.3	140	0.147	0.117	84.42	1.92
packed bed + 2.05g H ₂ O	275.65	2.7	525	0.137	0.057	79.00	1.79
	277.65	2	1545	0.094	0.042	53.84	1.22
5 mm SSB	273.65	2.7	1794	0.054	0.024	30.87	3.51
packed bed + 10.25g H ₂ O	275.65	2	1794	0.035	0.014	20.13	2.30
2 mm SSB packed bed + 2.05g H ₂ O	273.65	3.3	95	0.147	0.146	84.42	1.92

^avolume of hydrate at the end of the experiment.

The density of CH₄ hydrate is assumed as 0.9 g.cm⁻³.

$$VH = \frac{m_{wc}}{0.9}; m_{wc} = \Delta n_{hyd} \times M_w \times hydration\ number.$$

m_{wc} = mass of water consumed and M_w = molar mass of water

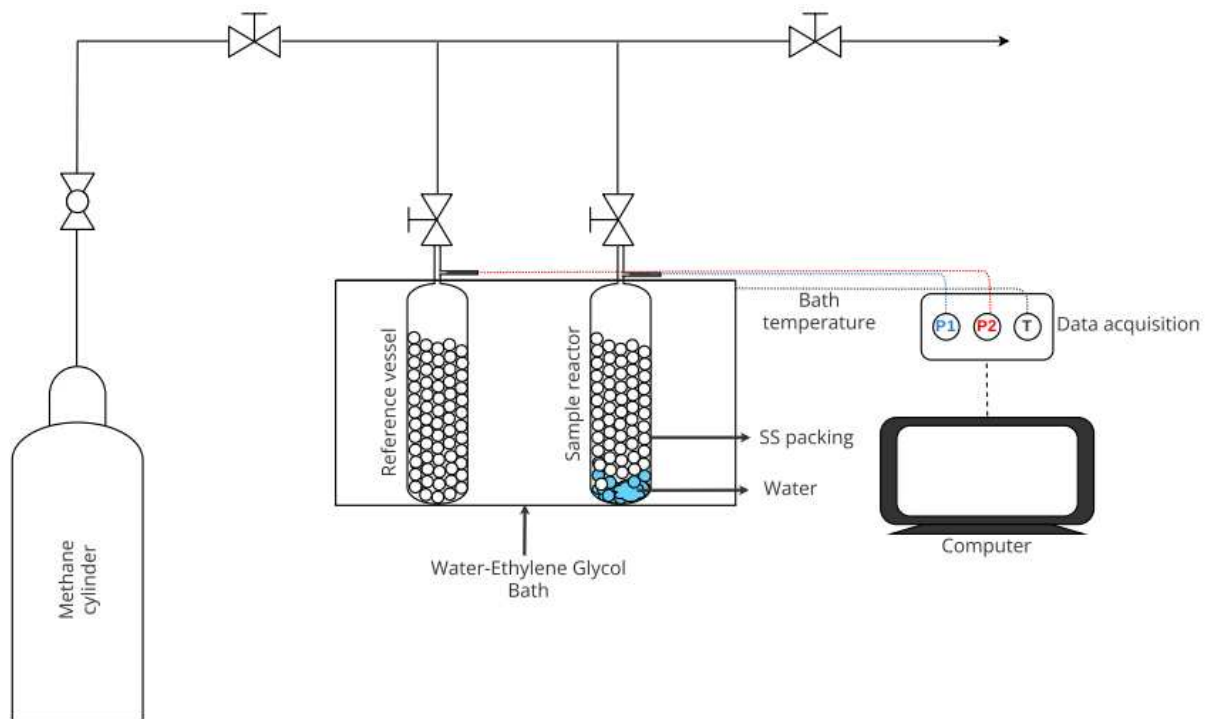


Figure 1. The schematic of the experimental setup for the study of CH₄ hydrate formation in SSB packing media

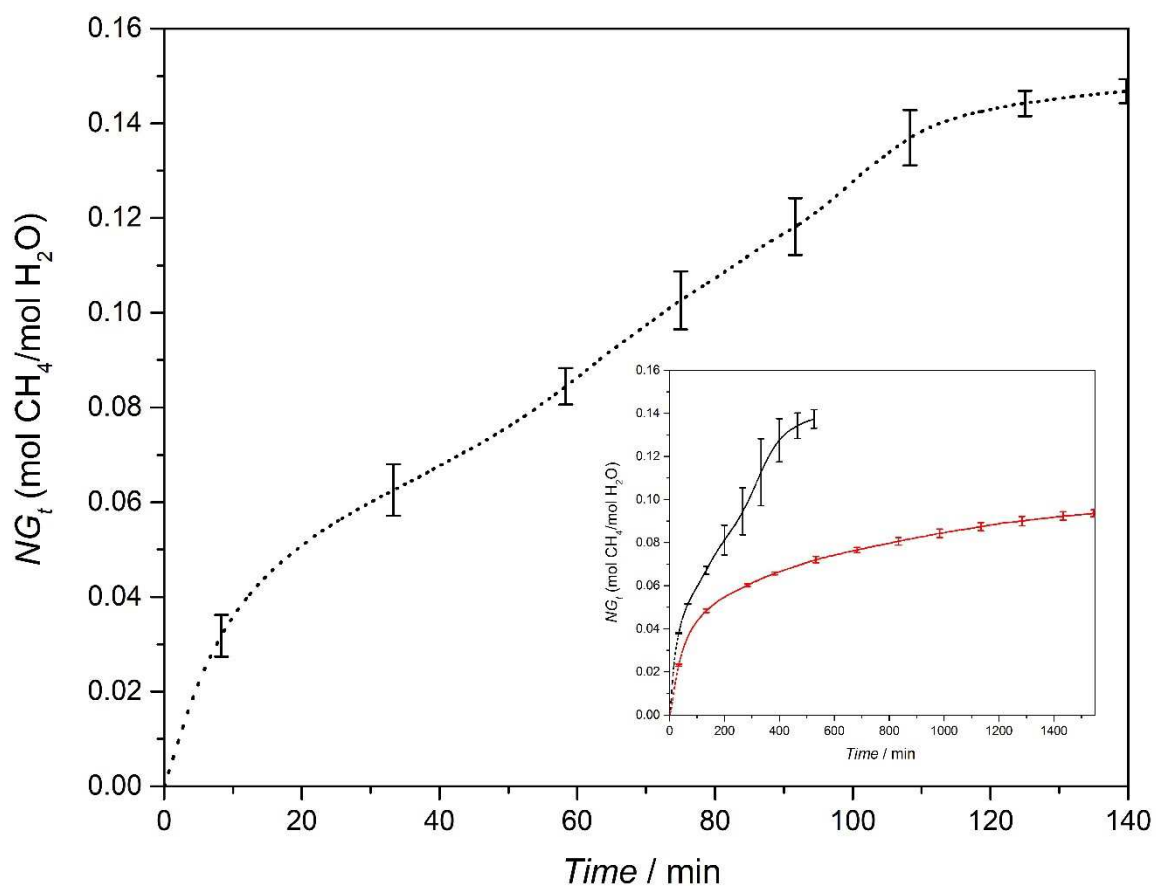


Figure 2. Average CH₄ uptake profile during hydrate formation experiments conducted at 273.65 K in a 5 mm SSB packed bed filled with 2.05g H₂O. Time zero corresponds to nucleation point. Inset: Average CH₄ uptake profile during hydrate formation experiments conducted at 275.65 K (black) and 277.65 K (red)

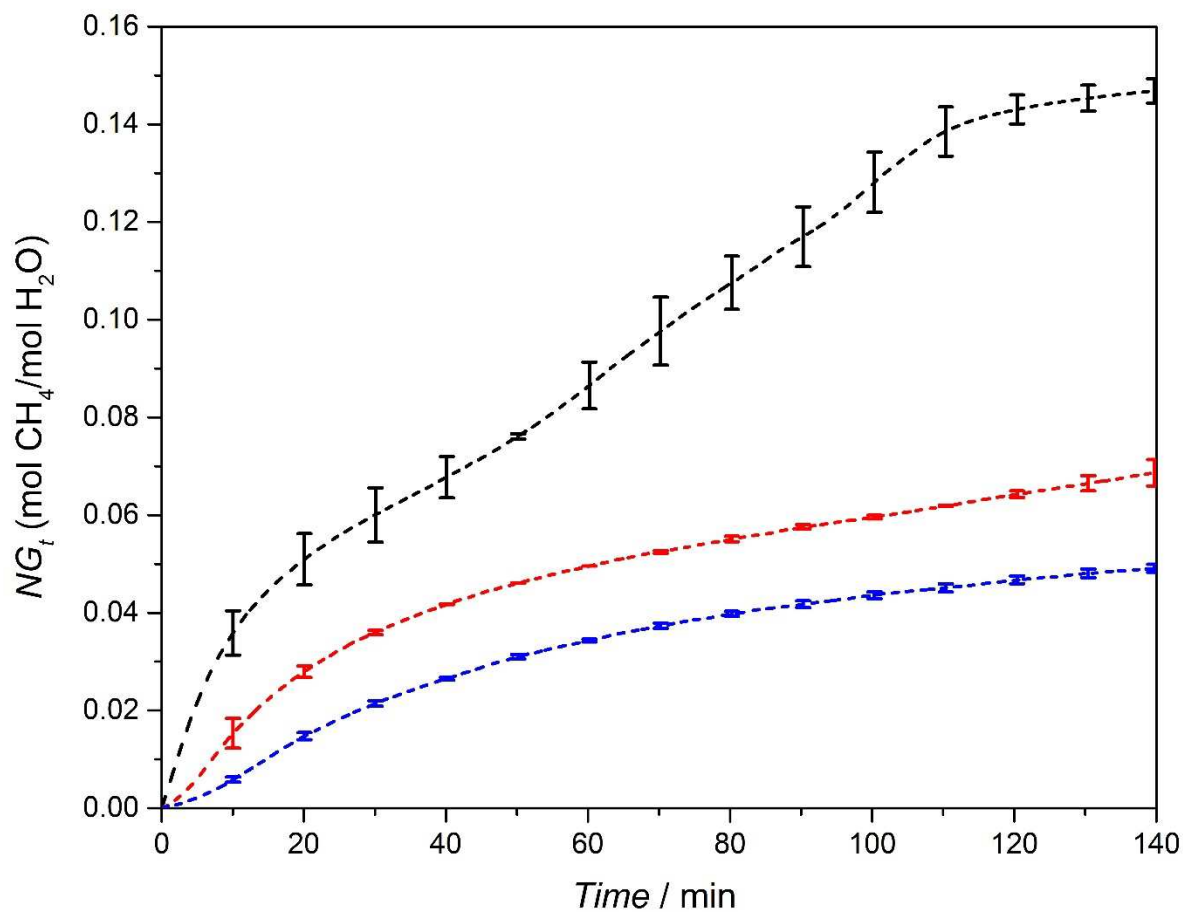


Figure 3. Comparison of average CH₄ uptake profile during hydrate formation experiments conducted at 273.65 K (black) and 275.65 K (red) 277.65 K (blue) in a 5 mm SSB packed bed filled with 2.05g H₂O. Time zero corresponds to nucleation point

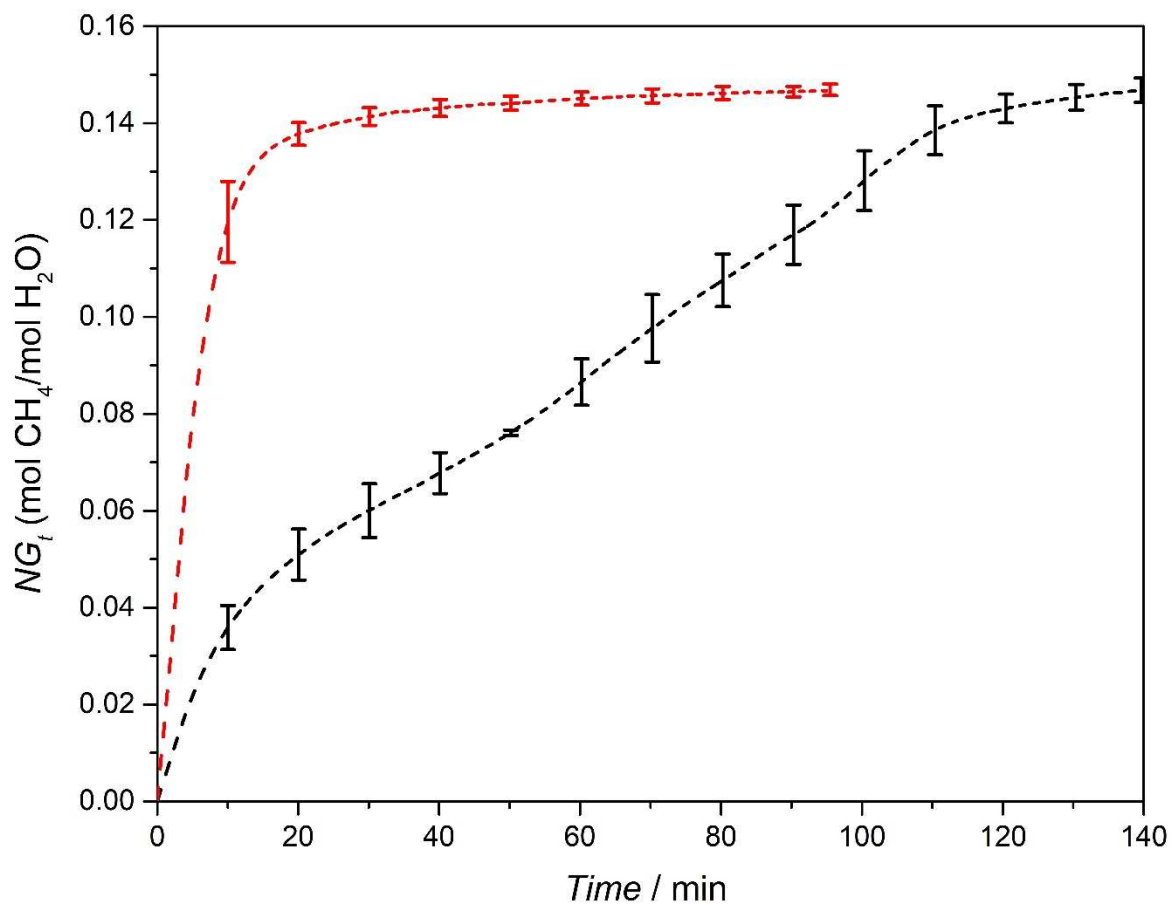


Figure 4. Comparison of CH₄ hydrate formation behavior at 273.65 K in 5 mm SSB packed bed (black) and 2 mm SSB packed bed (red) filled with 2.05g H₂O. Time zero corresponds to nucleation point

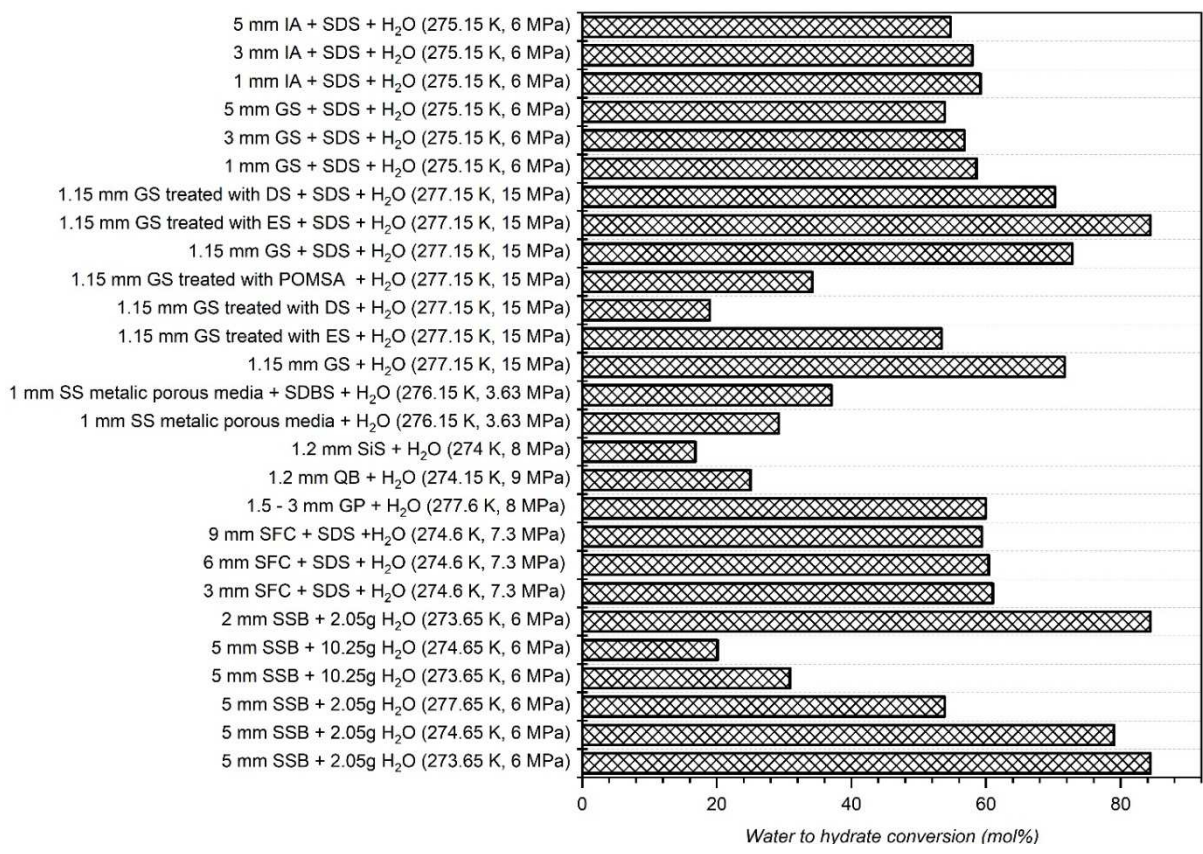


Figure 5. Comparing water to hydrate conversion (mol%) between different fixed packing materials with particle diameters greater than 1 mm (data compiled from [107, 141, 196-200]). IA: inert alumina, GS: glass spheres, ES: ethyltriethoxysilane, DS: *n*-dodecyltriethoxysilane, SDS: sodium dodecyl sulfate, POMSA: peroxymonosulfuric acid, SS: stainless steel, SDBS: sodium dodecyl benzenesulfonate, SiS: Silica sand, GP: granular Pebble, QB: quartz beads, SFC: SiC foam ceramic, SSB: stainless steel beads

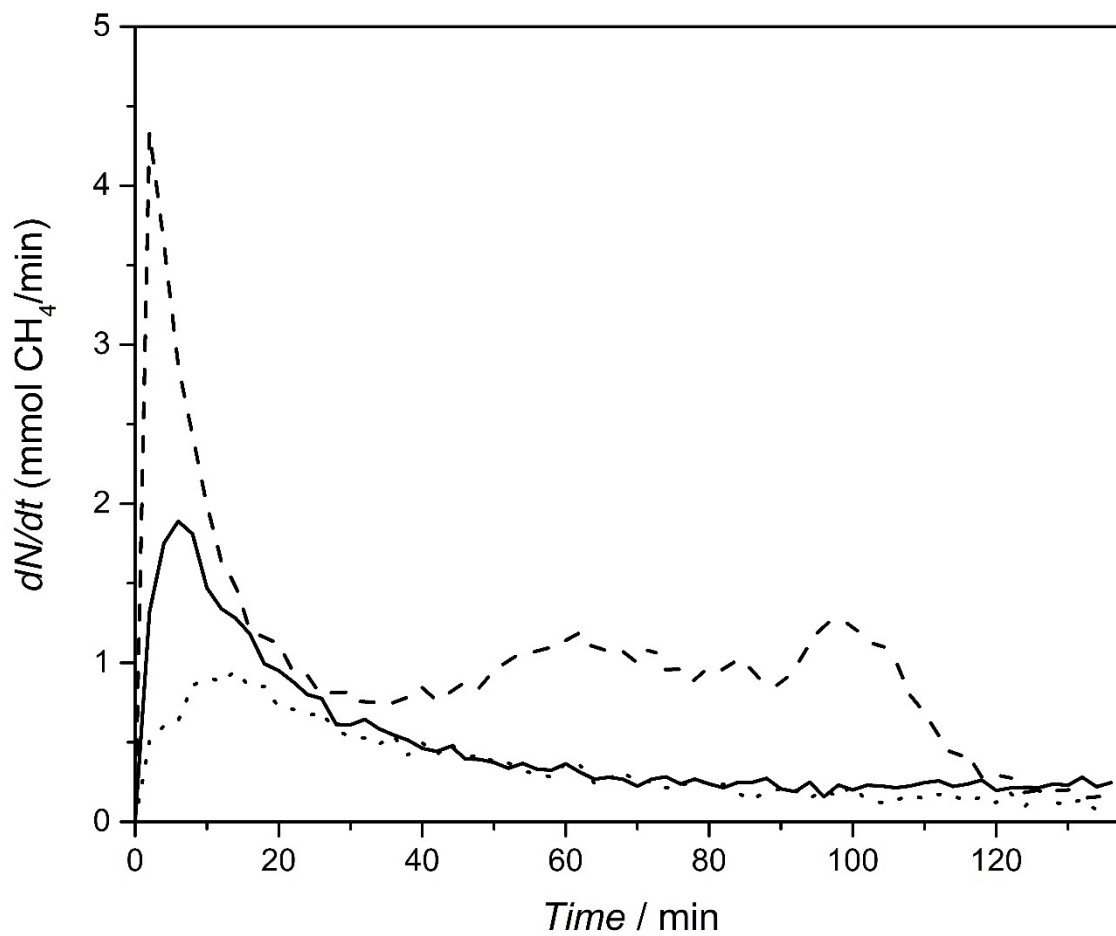


Figure 6. Rate of CH_4 hydrate formation at different driving forces; 3.3 MPa (dash), 2.7 MPa (solid), 2 MPa (dot) in 5 mm SSB packed bed filled with 2.05g H_2O

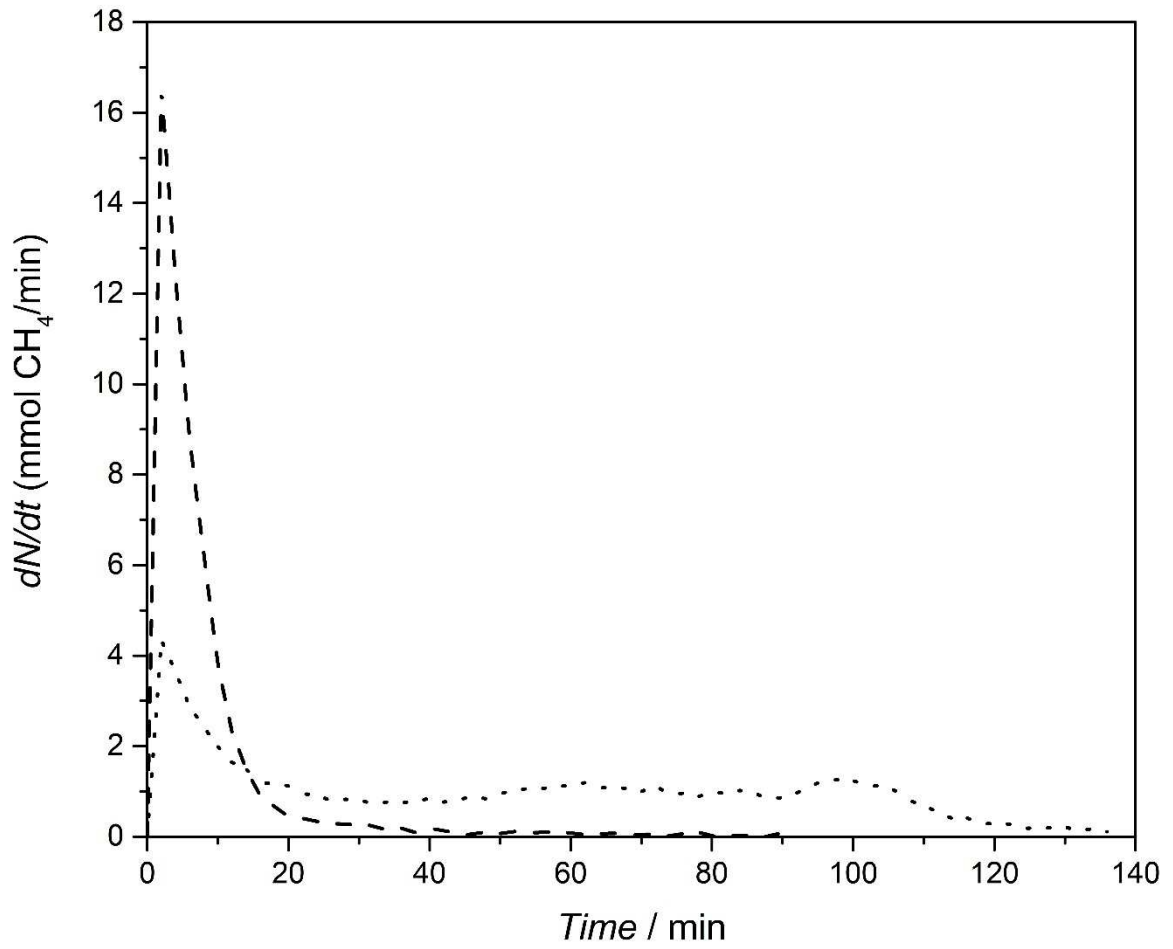


Figure 7. Rate of CH₄ hydrate formation in 2 mm SSB packed (dash) and 5 mm SSB packed (dot) bed filled with 2.05g H₂O at a driving force of 3.3 MPa

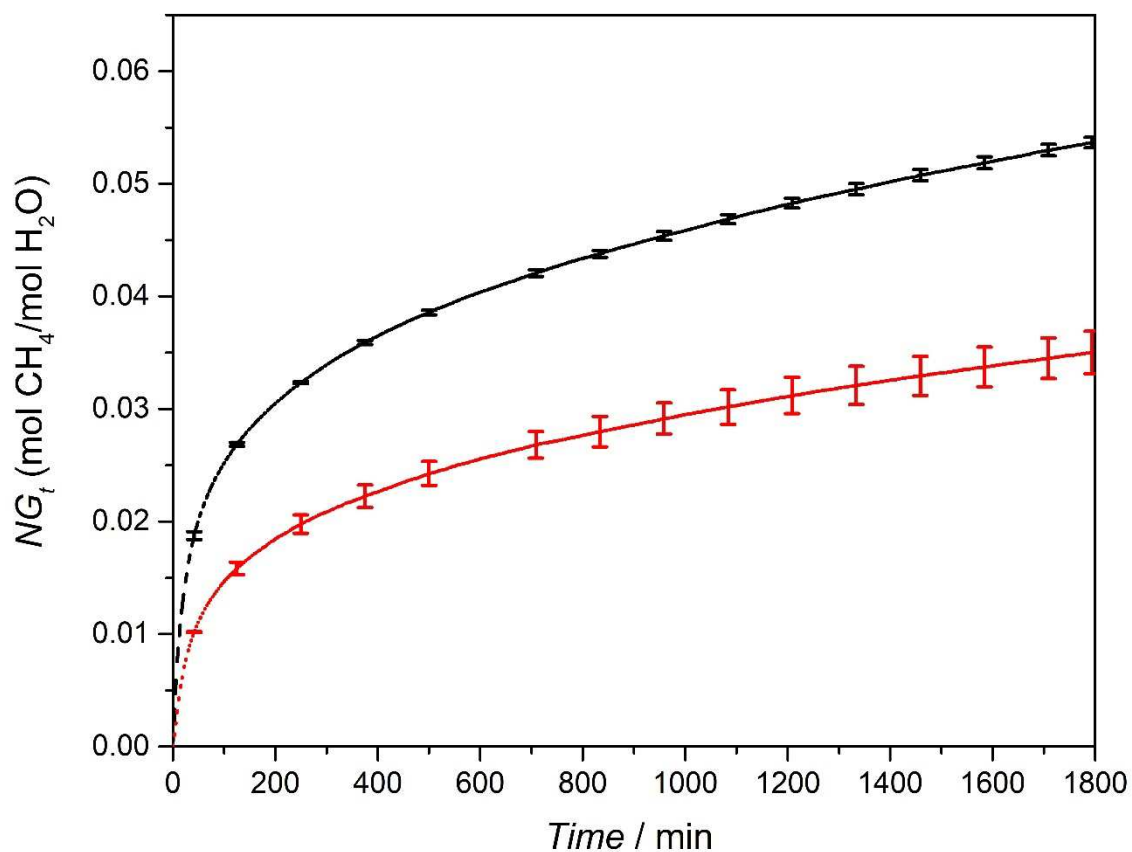


Figure 8. CH_4 gas uptake measurements for the experiments conducted at 273.65 K (black) and 275.65 K (red) in a 5 mm SSB packed bed filled with 10.25g H_2O and with an initial pressure of 6 MPa

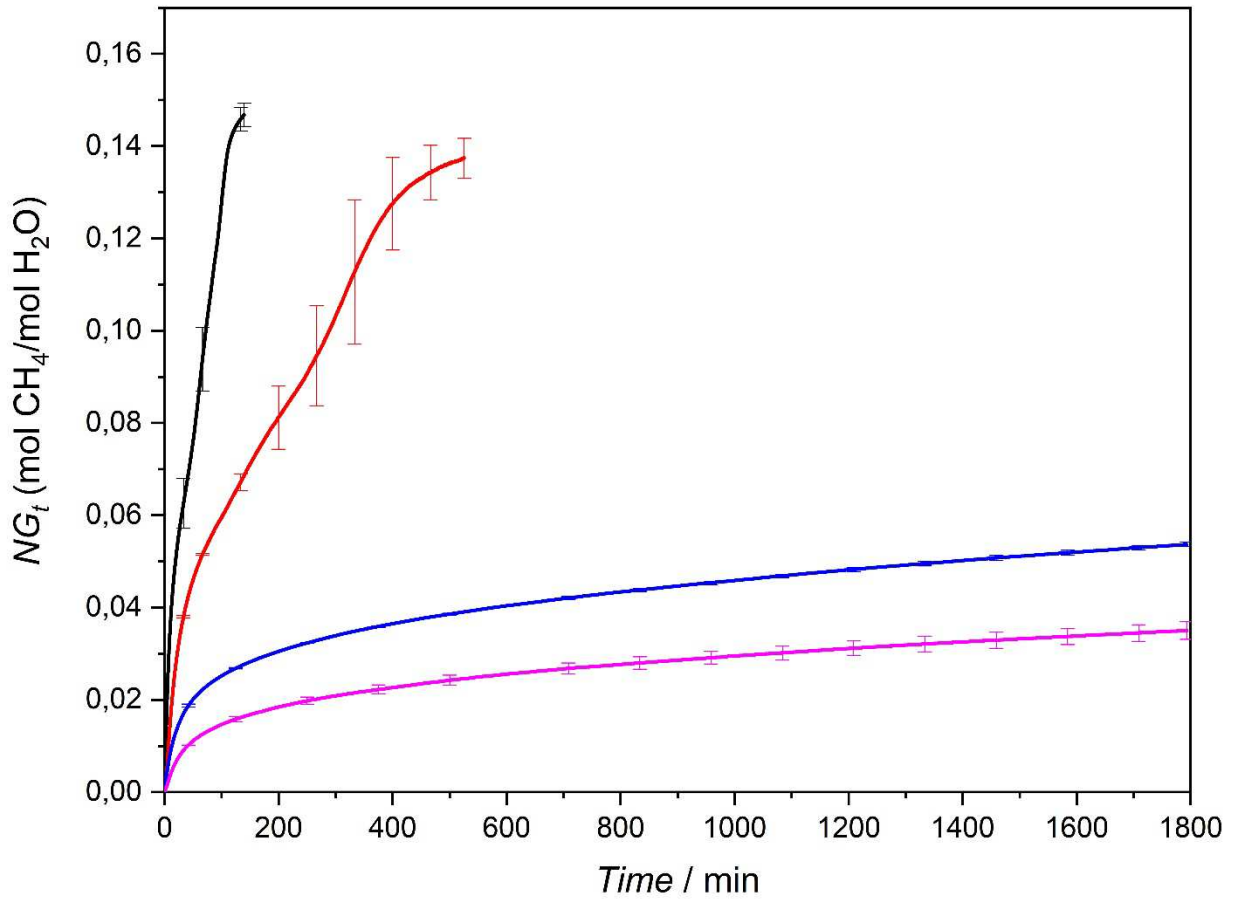
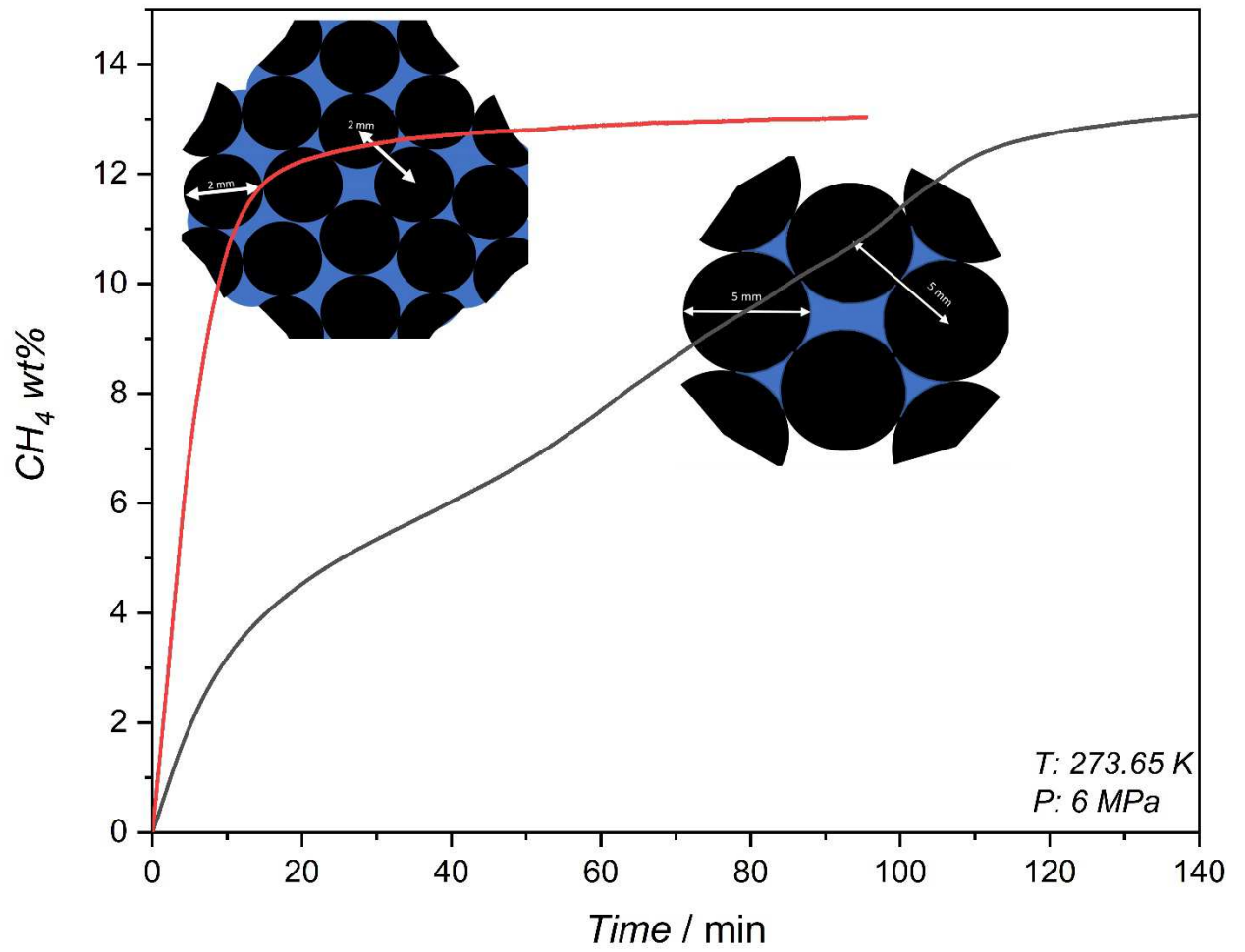


Figure 9. Normalized gas uptake measurements for the experiments conducted at 273.65 K and 275.65 K in a 5 mm SSB packed bed filled with 2.05 g and 10.25 g H₂O. Black: (2.05 g H₂O – 273.65 K), Red: (2.05 g H₂O – 275.65 K), Blue: (10.25 g H₂O – 273.65 K), Magenta: (10.25 g H₂O – 275.65 K)



TOC